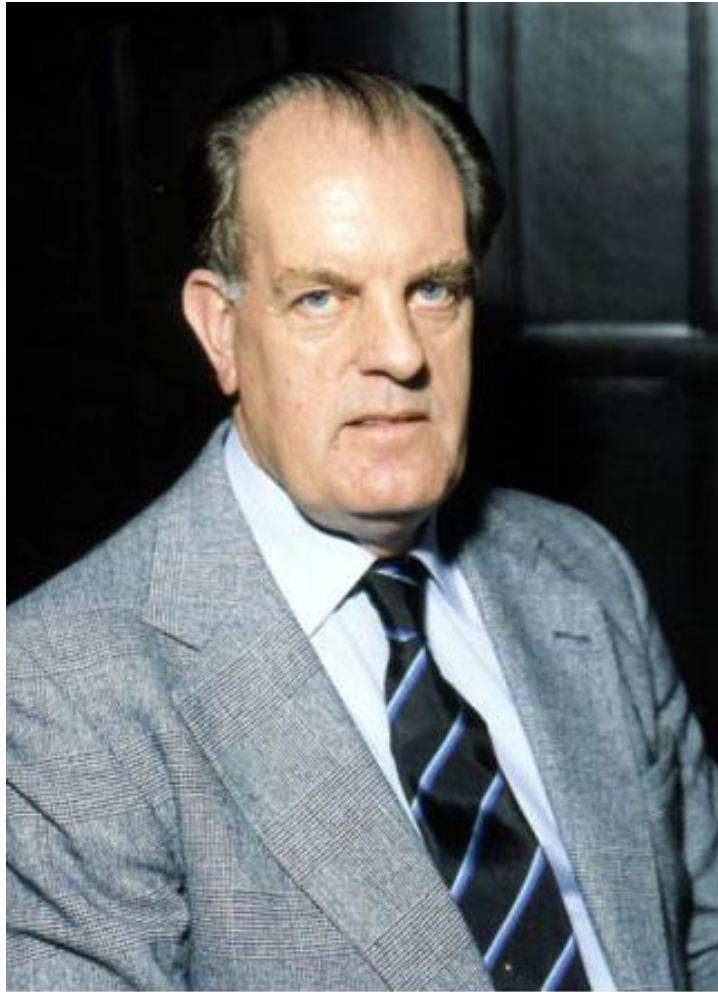


Lessons learned from
Cambridge (UK) Soil Models.
Andrew N. Schofield GeoVirginia 2013
Trench & Tunnel heading damage

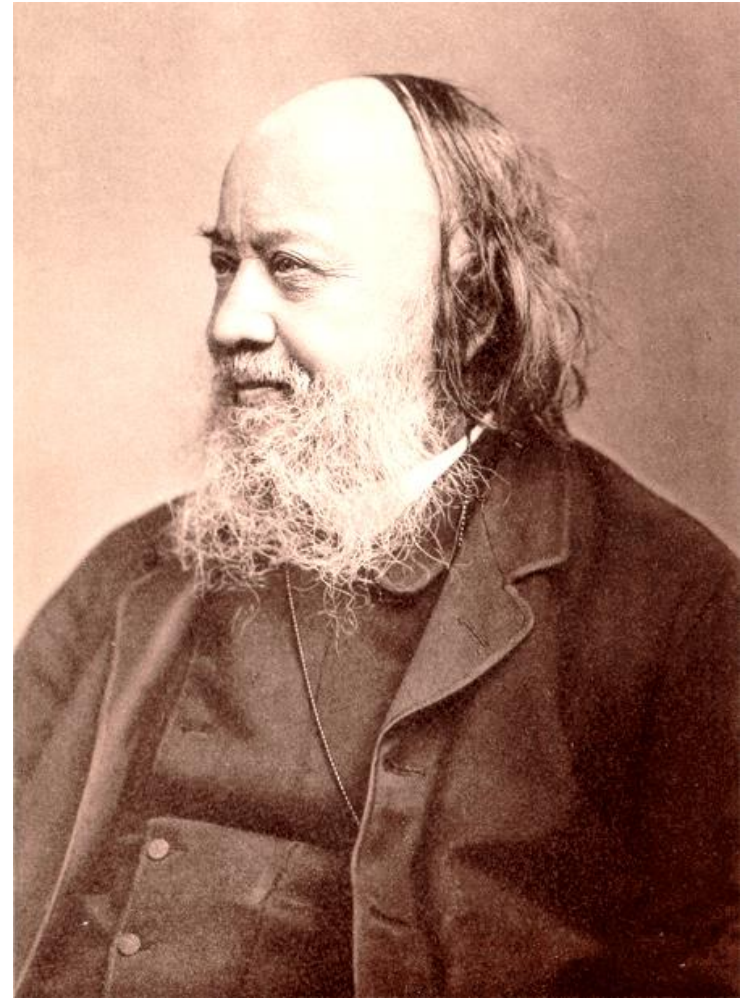
- 1) Tunnel faces can be supported by compressed air, or as in Crossrail, by earth pressure balance.
- 2) A trench for a sewer pipe with a backdrop has a deep cut face without heading support pressure.
- 3) Centrifuge model tests with authentic soil states revealed new heading damage mechanisms.



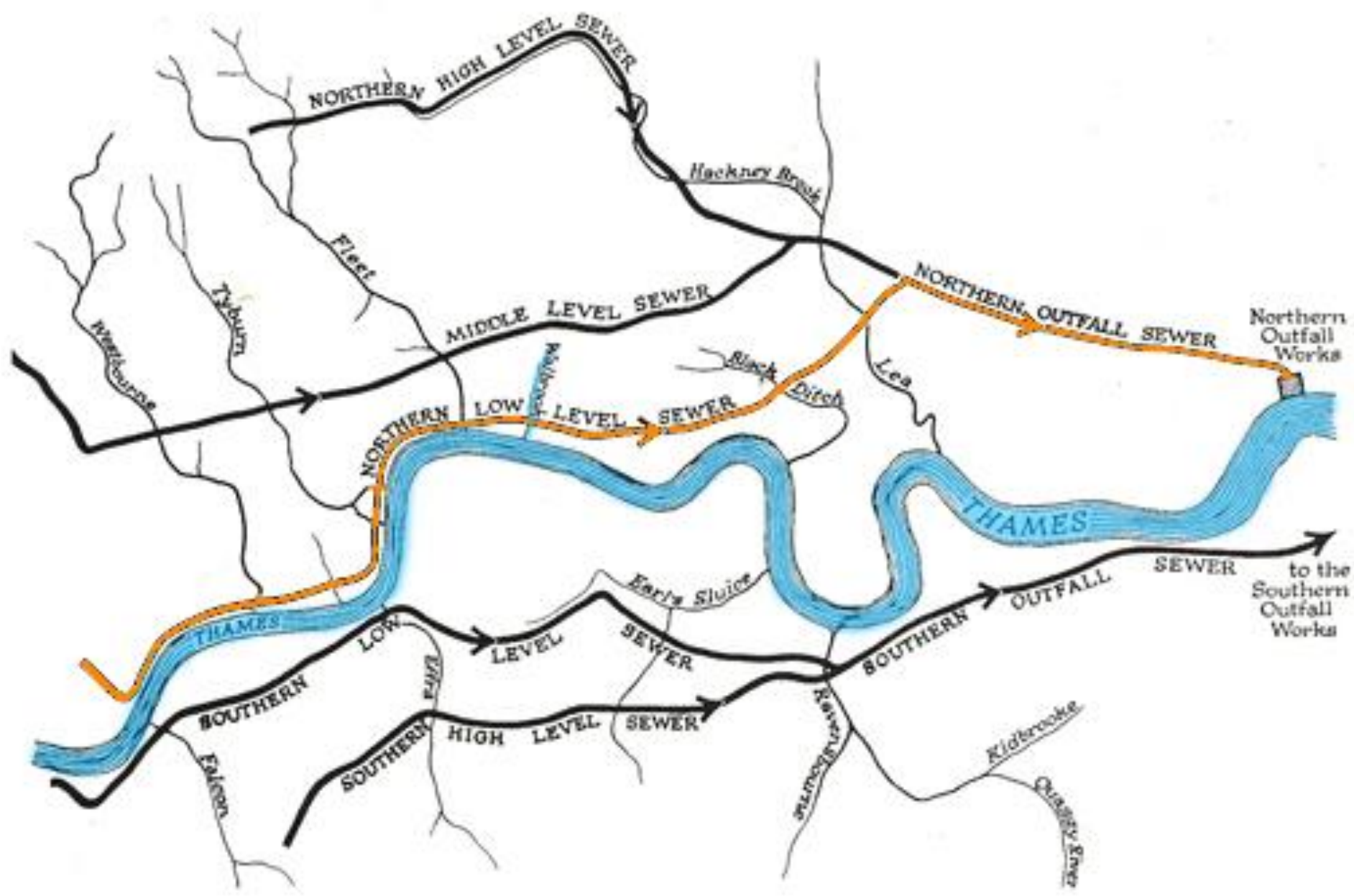
Crossrail – 550 tonne tunnelling machine Elizabeth being lowered into 40m deep shaft at Limmo Peninsula



Sir Denis Rooke
1924-2008

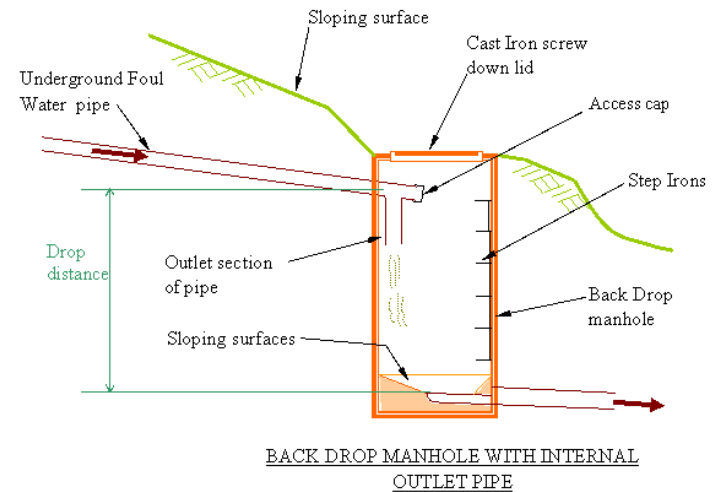


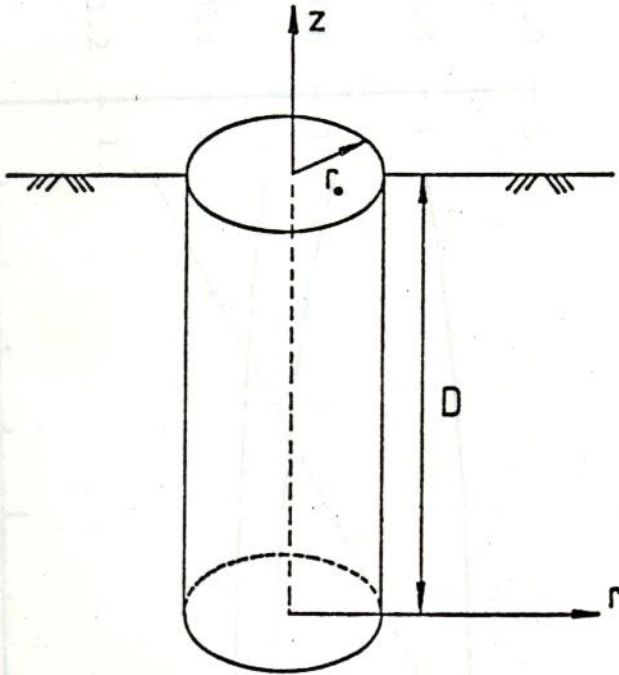
Sir Edwin Chadwick
1800-1890



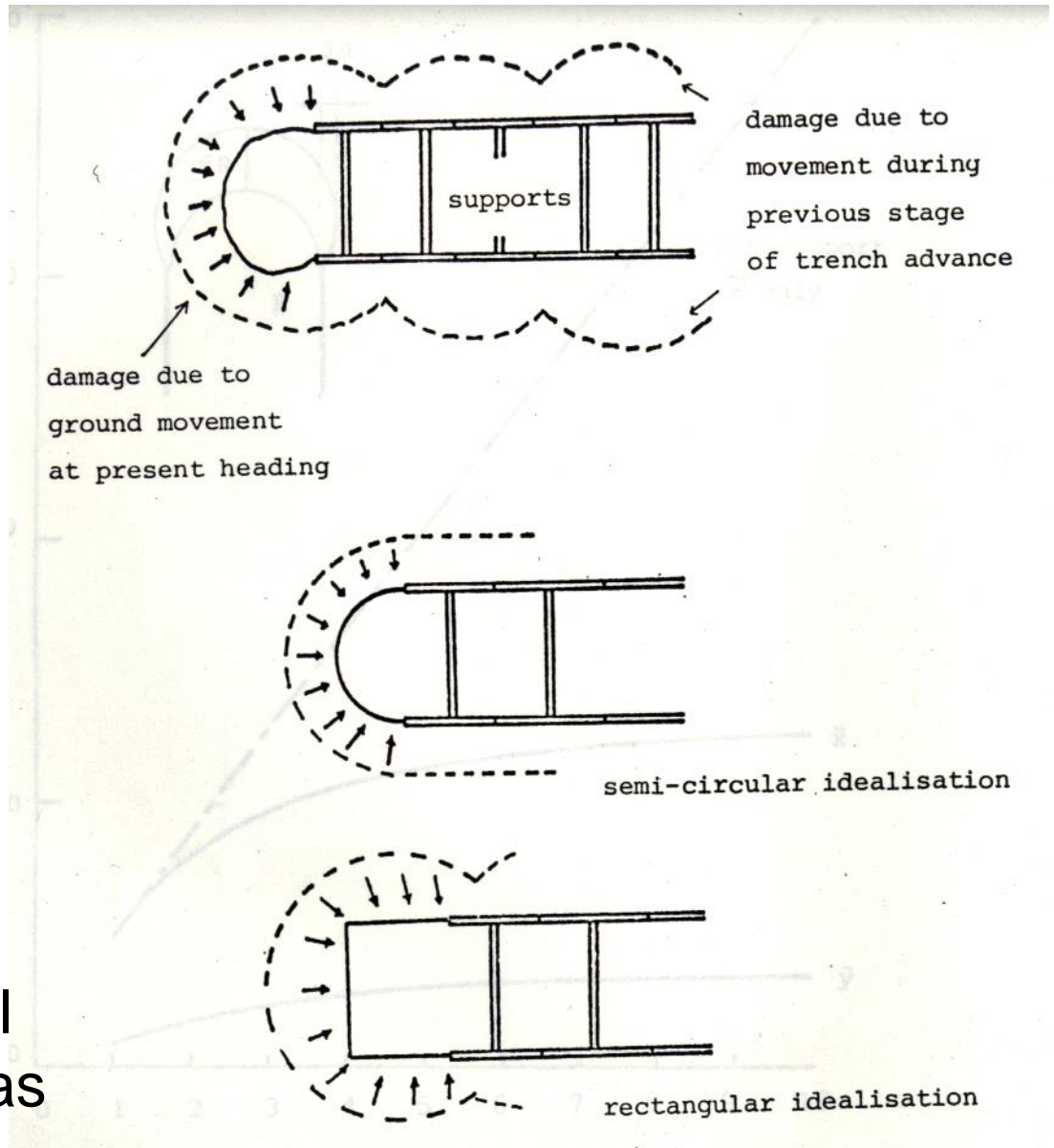
Bazalgette's sewer system. Image: N. Barton, "Lost Rivers of London" (Modified)

A backdrop will reduce sewer flow rate, but will cause deep trench-heading damage





Kusakabe's model tests for British Gas



Alternative soil strength models and theories

Terzaghi's Equation

Strength on a slip surface
 =(slip friction)+(cohesion).
 $\tau = \sigma' \tan \phi' + c'$

$$\tau = \sigma' \tan \phi' + c'$$

Taylor's CS+Interlocking

$$\tau = \sigma' \tan \phi_d + \sigma' (dy/dx)$$

Cam-clay Strength

=(aggregate CS friction) +
 (interlocking).

An increment $d\varepsilon$ of plastic distortion unloading and reloading soil grains will dissipate "frictional" work
 $dW = M p' d\varepsilon$.

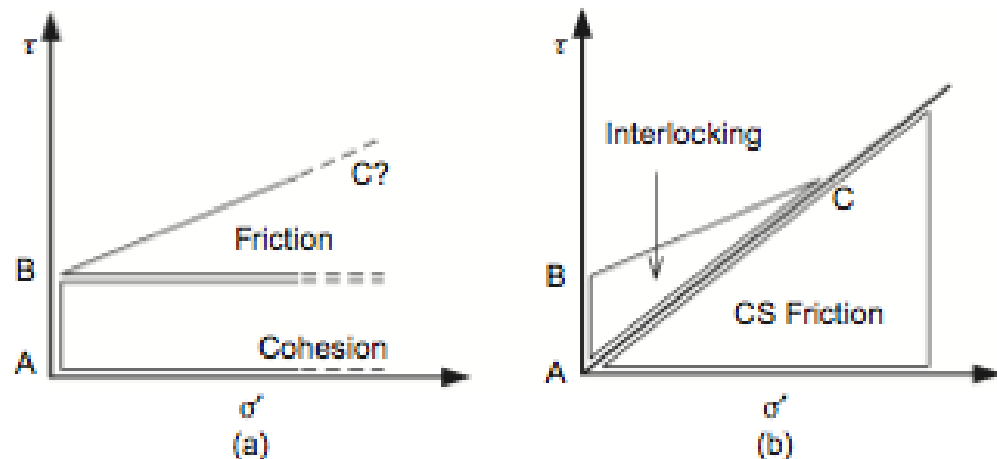


Fig. 1. Alternative models for soil strength

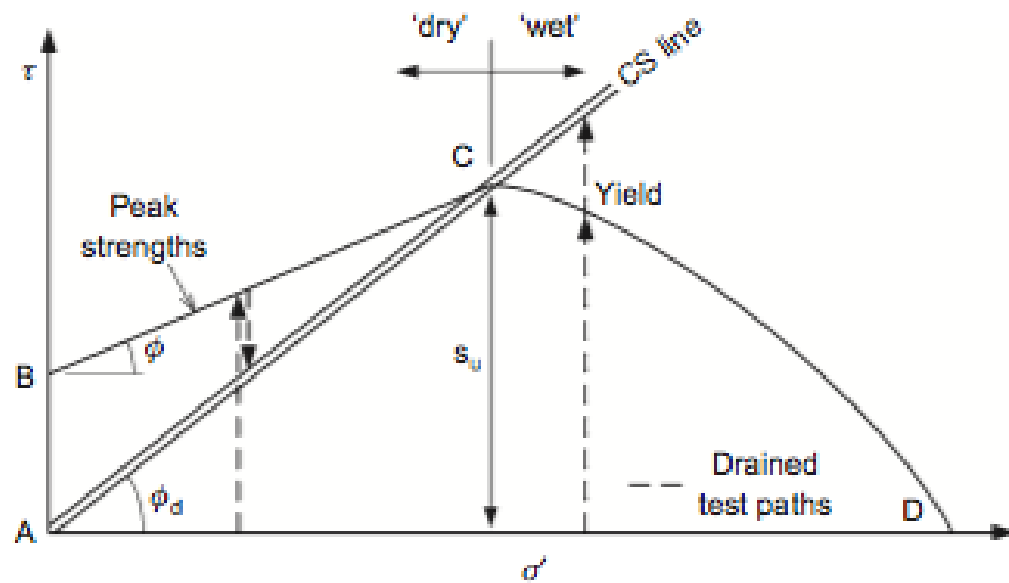


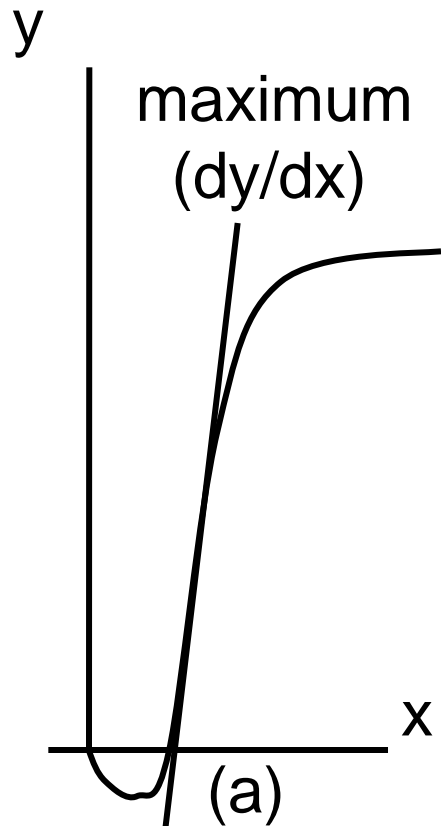
Fig. 2. Observed soil behaviour, in critical state framework

Grain-aggregate mechanics in typical slopes at rest.

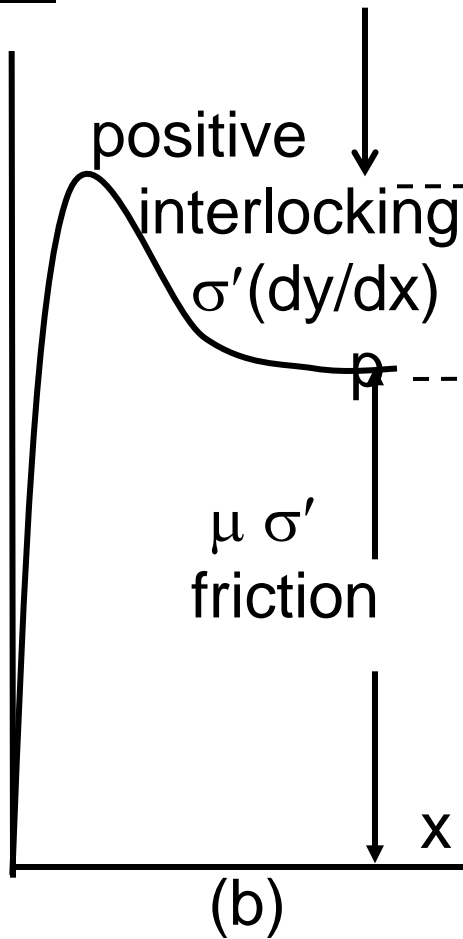
- The typical effectively stressed grain-aggregate in CS critical states with $v_\lambda = v + \lambda \ln p' = \Gamma$ is a heap of sand at rest in an hour-glass.
- No dust is seen in an hour glass. Any grain damage would have made dust hence internal-friction in sand must dissipate energy by elastic collisions of grains without damaging the grains.



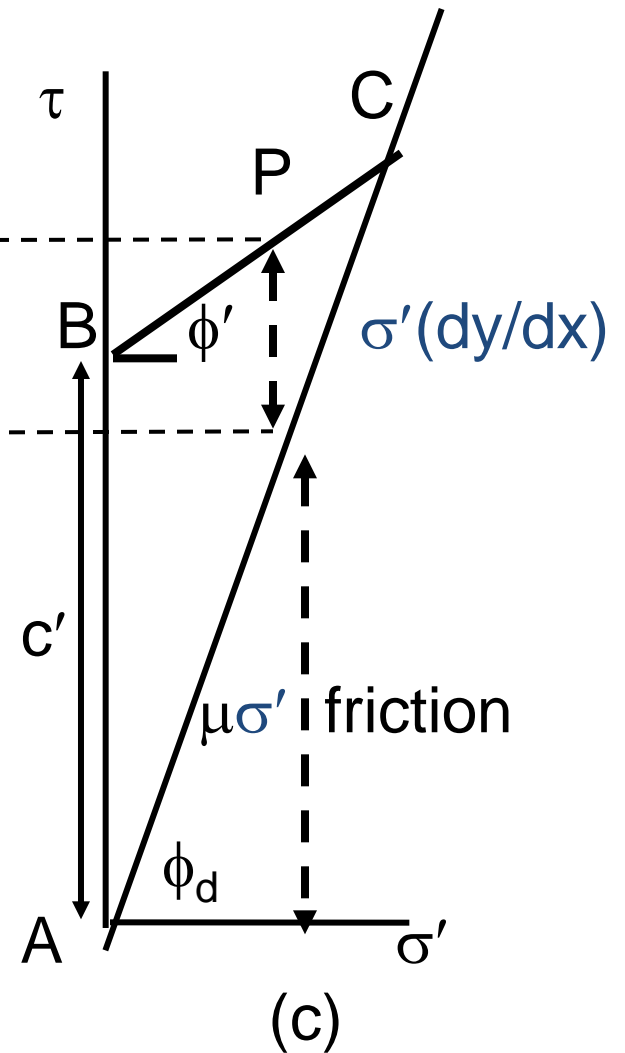
Interlocking in Taylor's MIT shear box tests



Taylor's interlocking strength component.
 $\tau = \mu \sigma' + \sigma'(dy/dx)$



strength = friction + interlocking



Peak drained strength at P; see Schofield (2006) Géotechnique