

Challenges in the Design of Screw-Piles and Helical Anchors in Soils

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Outline

What are Screw-Piles and Helical Anchors?

Challenge 1. Characterization of Soil Parameters

Challenge 2. Understanding Effects of Installation
Disturbance

Challenge 3. Understanding Role of Shaft & Helix

A Comment on Torque-to-Capacity Ratios

International Building Code

Section 1802.1 defines a Helical Pile as:

“Manufactured steel deep foundation element consisting of a central shaft and one or more helical bearing plates. A helical pile is installed by rotating it into the ground. Each helical bearing plate is formed into a screw thread with a uniform defined pitch.”



This Technology is Not New

It is Over 170 Years Old

1st Recorded use of Screw-Piles was by Alexander Mitchell (1780-1868) in 1836 for Ship Moorings and was then applied by Mitchell as Foundations for Maplin Sands Lighthouse in England in 1838

Mitchell's Screw-Pile Specifications for Maplin Sands

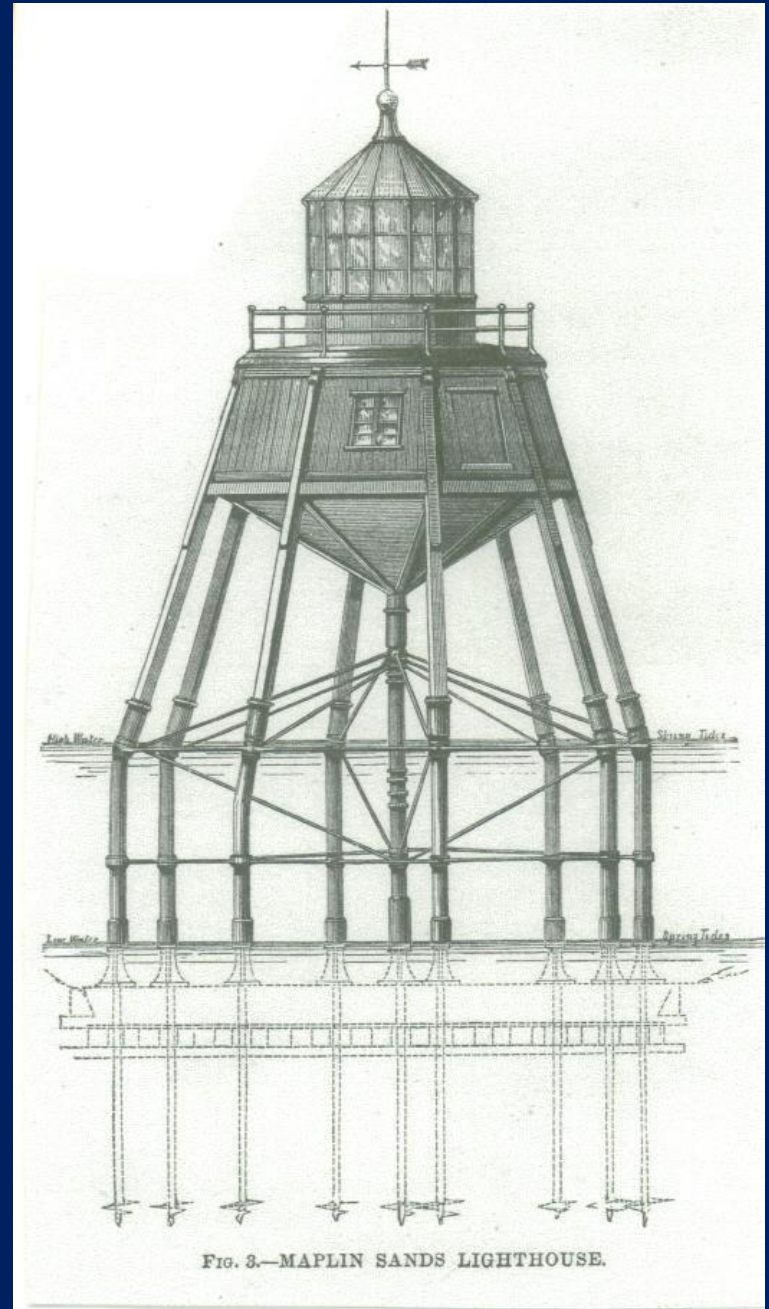
Material – Cast Iron

Shaft Diameter – 5 in.

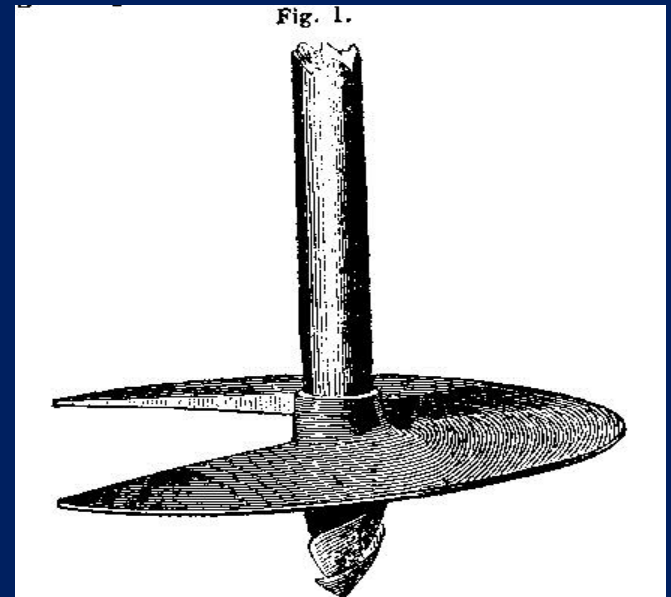
Screw (Helix) Diameter – 4 ft.

Depth Below “Mudline” – 12 ft.

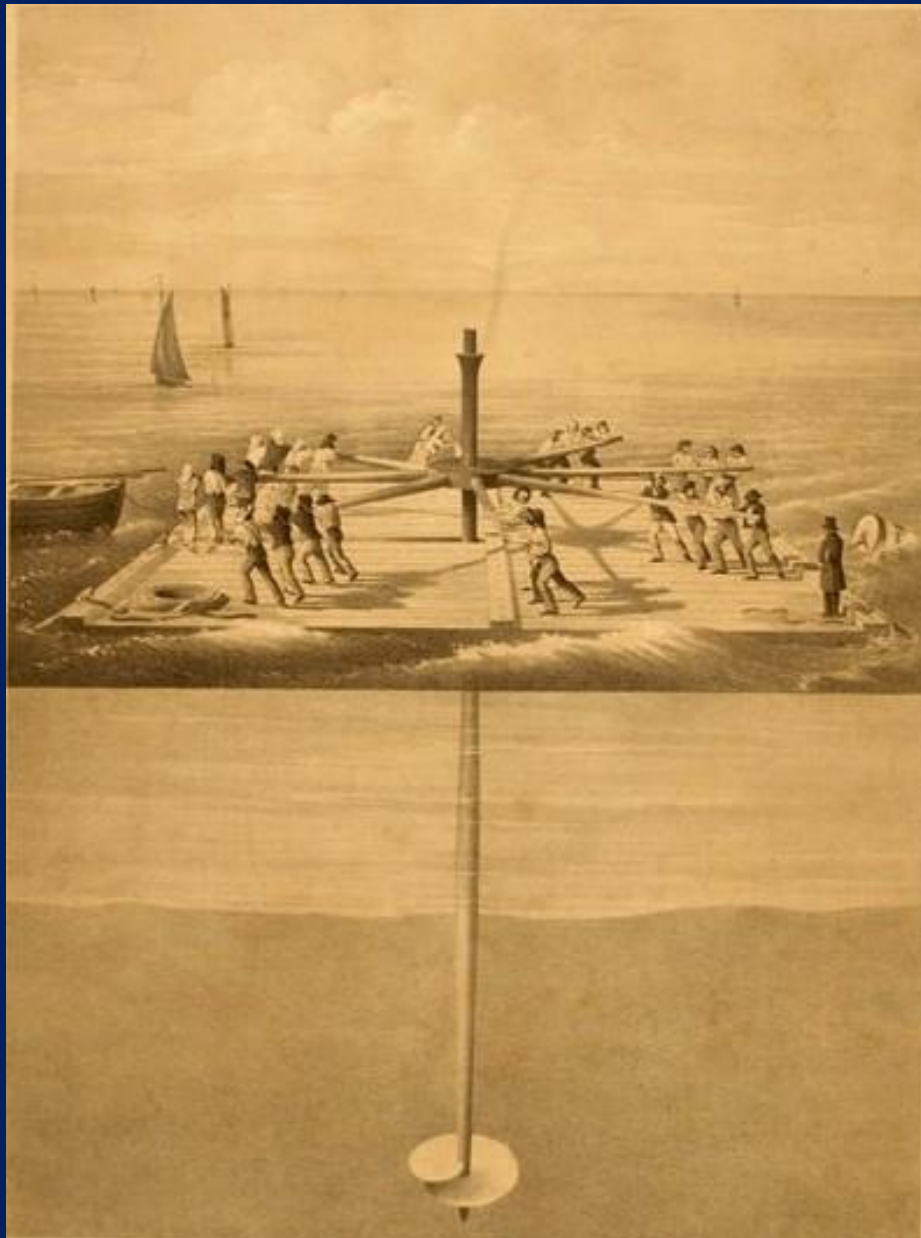
Orientation - Vertical



“On Submarine Foundations;
particularly Screw-Pile and
Moorings”, by Alexander
Mitchell, Civil Engineer and
Architects Journal, Vol. 12,
1848.

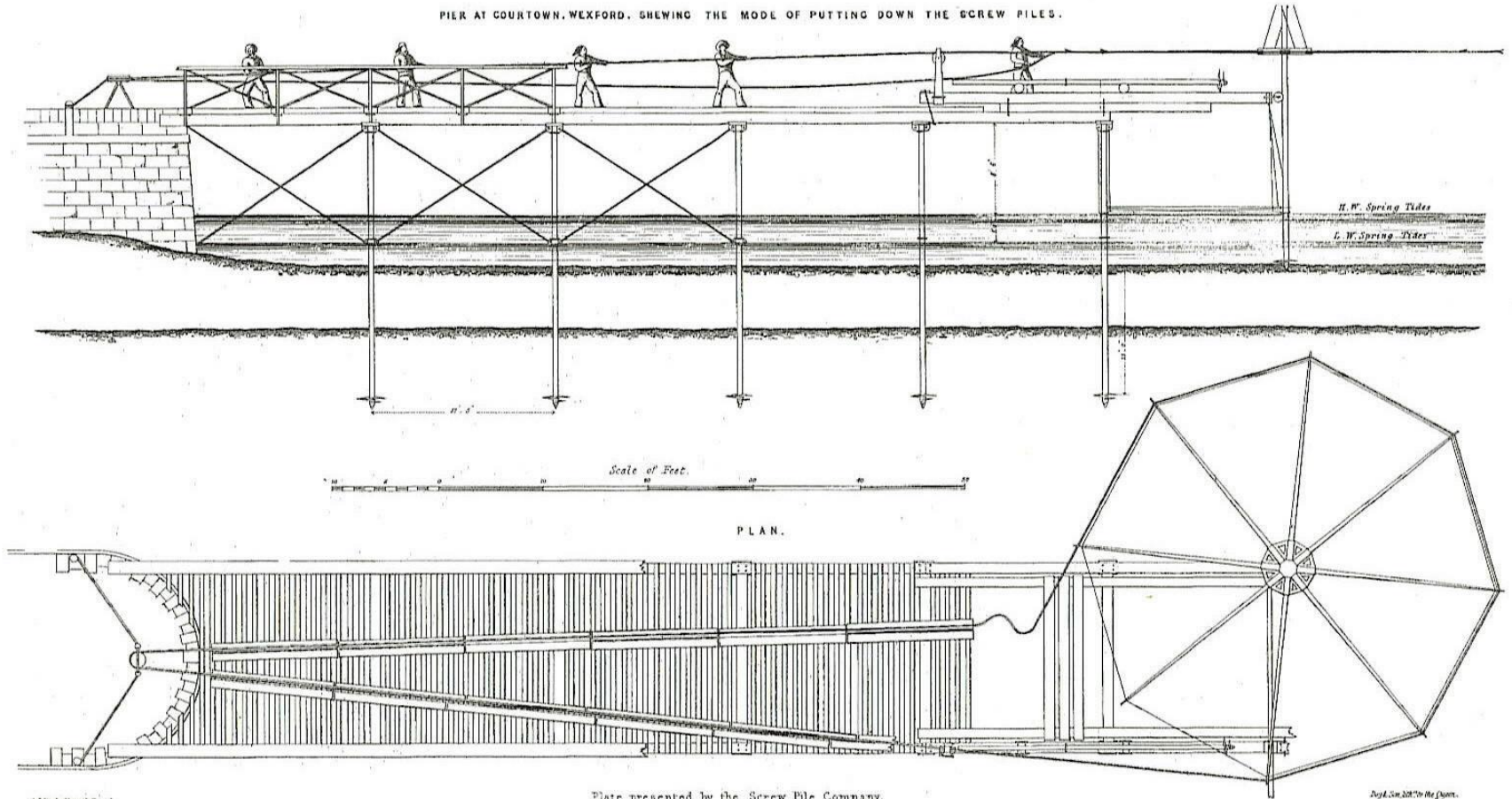


“ Whether this broad spiral flange, or “Ground Screw,” as it may be termed, be applied ... to support a superincumbent weight, or be employed ... to resist an upward strain, its holding power entirely depends upon the area of its disc, the nature of the ground into which it is inserted, and the depth to which it is forced beneath the surface.”

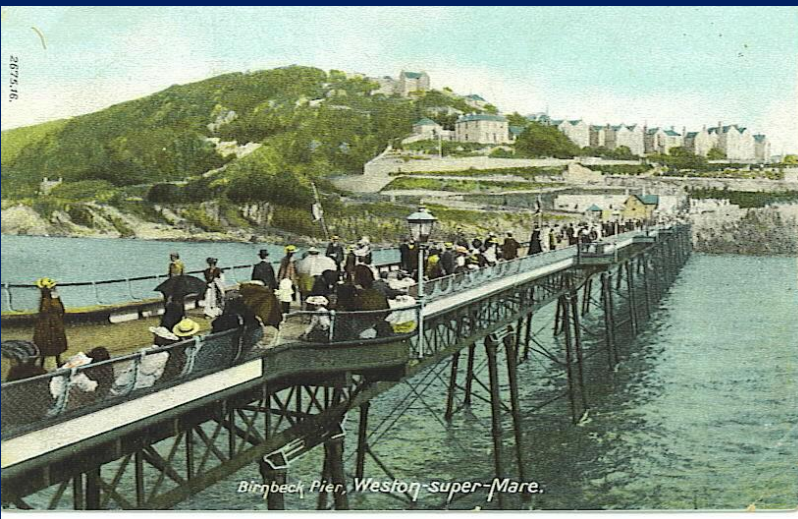


Pier Construction

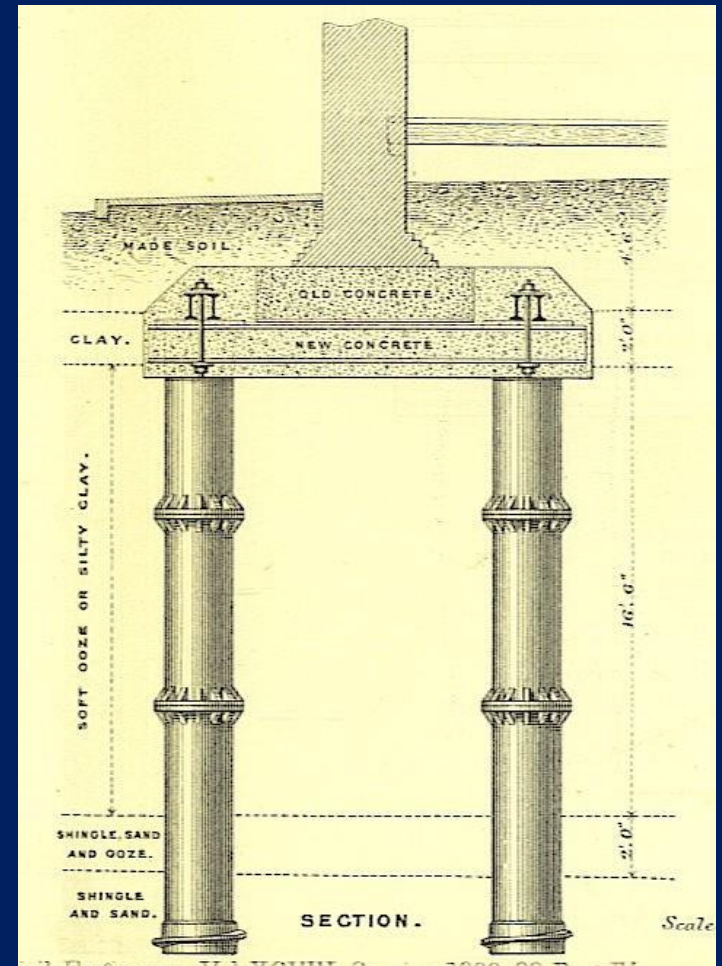
PIER AT COURTTOWN, WEXFORD, SHEWING THE MODE OF PUTTING DOWN THE SCREW PILES.



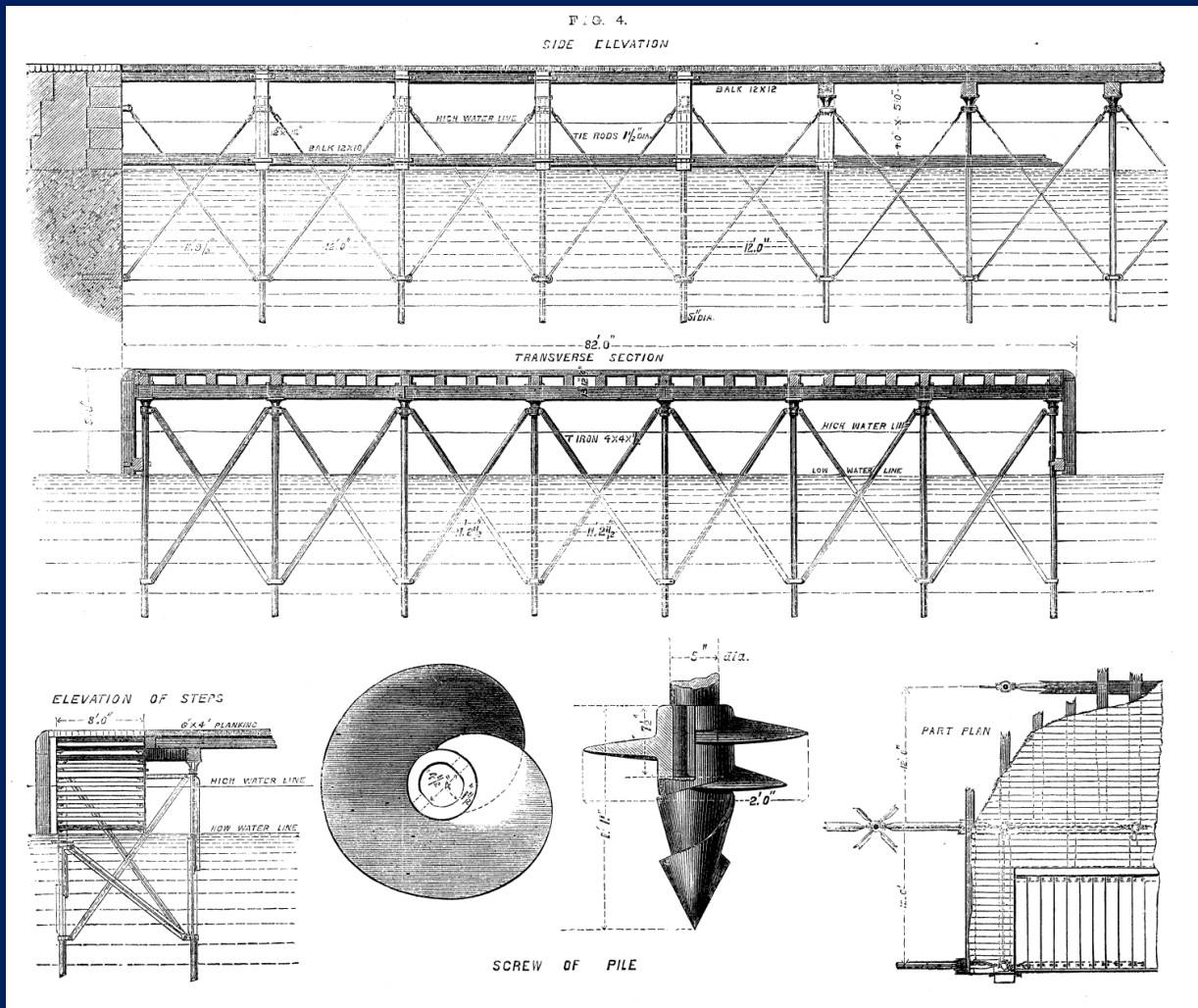
Pleasure Piers in England



Underpinning - Great Yarmouth Town Hall 1880



Bridge Foundations



How are Screw-Piles and Helical Anchors Currently Being Used in Civil Construction?

Electric Utilities

Underpinning/Retrofitting Existing
Foundations

New Foundations and Anchor Systems



Factory Manufactured Foundation/Anchor System

The Industry is Largely
Driven by Manufacturers and
Contractors

The Complexity of Design

Single-Helix or Multi-Helix?

“Tapered” or Uniform Helices?

Close or Large Helix Spacing?

Square-Shaft or Round-Shaft?

Compression or Tension?

Sand or Clay?

Steel Shaft or Grouted Shaft?

Aging

What are the Challenges in Design?

Challenge 1. Characterization of Soil Parameters

Challenge 2. Understanding Effects of Installation
Disturbance

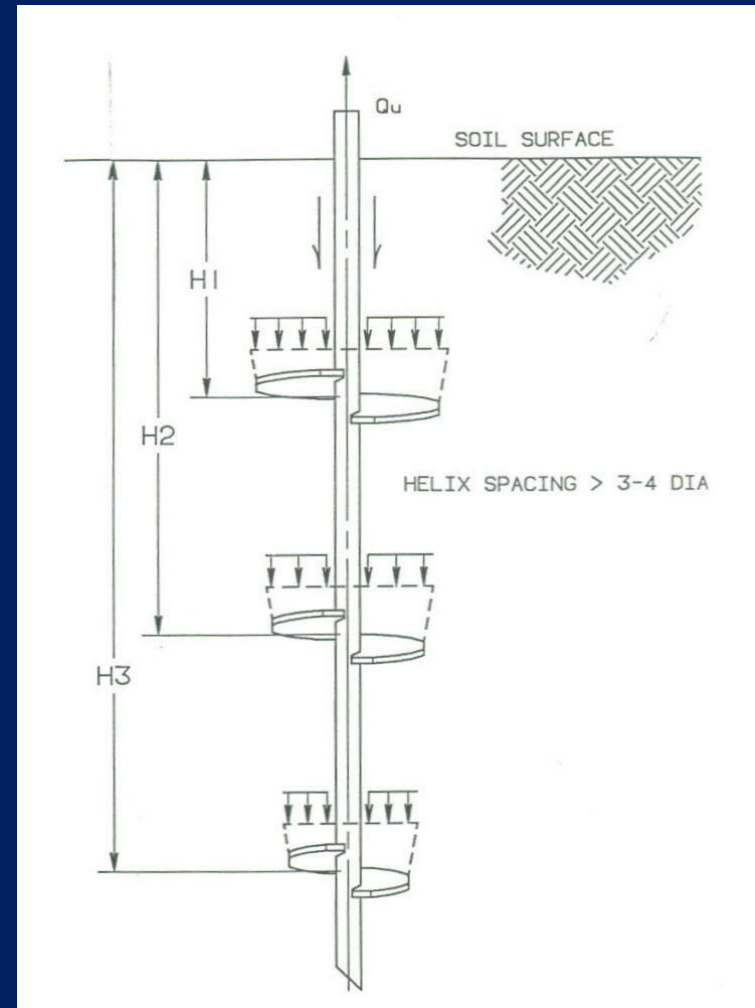
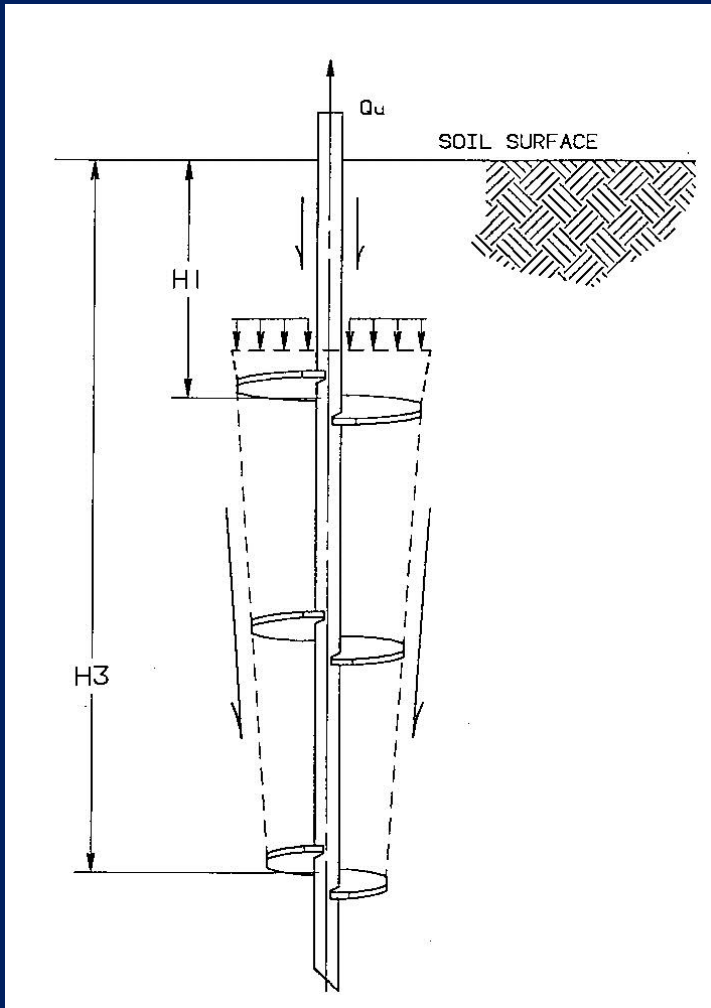
Challenge 3. Understanding Role of Shaft & Helix

Challenge 1. Characterization of Soil Parameters

Not Unique to Screw-Piles and Helical Anchors
but Needed for all Geotechnical Projects

We Need to Evaluate Models Used for Design
and Determine Input Parameters

Traditional Design Models



Evaluation of Ultimate Capacity (Traditional Soil Mechanics Approach)

Single-Helix

Clay – Undrained TSA

$$Q_H = s_u N_c A_H$$

Sand – Drained ESA

$$Q_H = N_q \sigma_v' A_H$$

Multi-Helix

$$Q_T = \sum Q_{HI}$$

In Uniform Soils with Same Size Helices

$$Q_T = N \times Q_{HI}$$

Now Include Shaft Resistance for Round Shafts

$$Q_T = \sum Q_{HI} + Q_S$$

$$Q_S = f_s A_S$$

$$f_s = s_u \alpha$$

$$f_s = \beta \sigma'_v$$

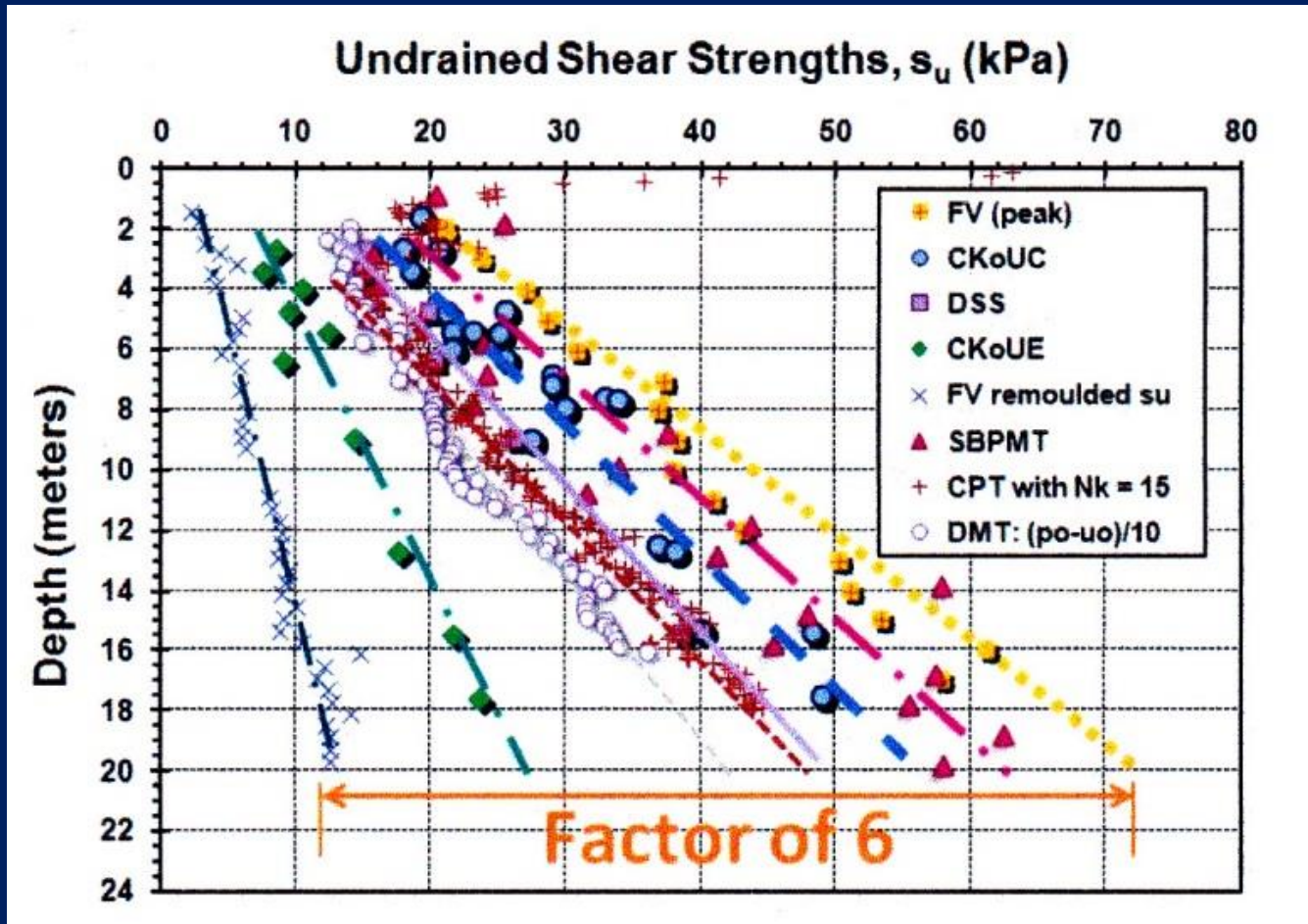


Other than Compositional
Characteristics, Most Soil Parameters are
Not Unique

Clay – Undrained Shear Strength:
but which s_u ??

Sand - N_q from ϕ' :
but which ϕ' and which N_q ?

Undrained Shear Strength of Clay from Different Tests (from Mayne)



N_q Chart from Popular Book

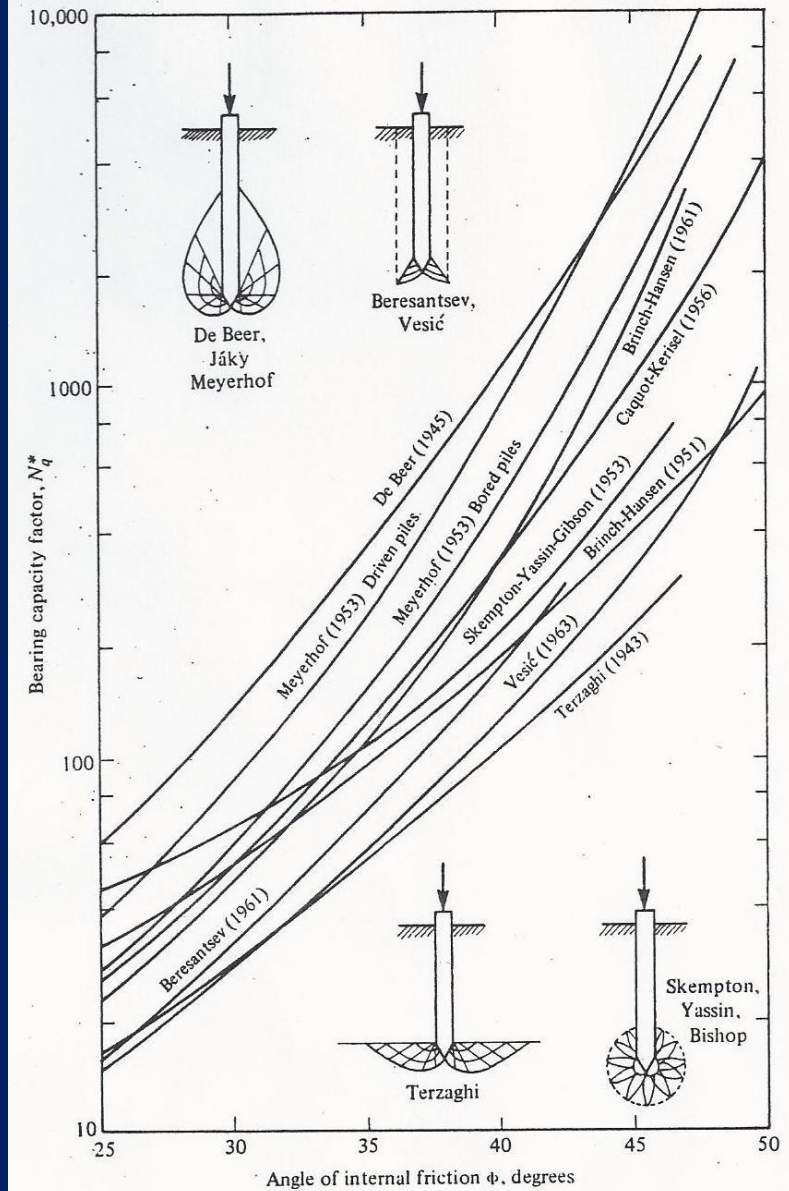


Fig. 19.49 Bearing capacity factors vs. angle of internal friction, according to various authors.

Challenge 2. Understanding Effects of Installation Disturbance (Related to Challenge 1)

Somewhat Unique to Screw-Piles and Helical
Anchors but Important for Many Deep
Foundations

We Need to Evaluate How Contractor
Installation May Affect Soil Parameters

Where Might We Expect Installation Disturbance and a Reduction in Helix Efficiency?

“Structured” Soils

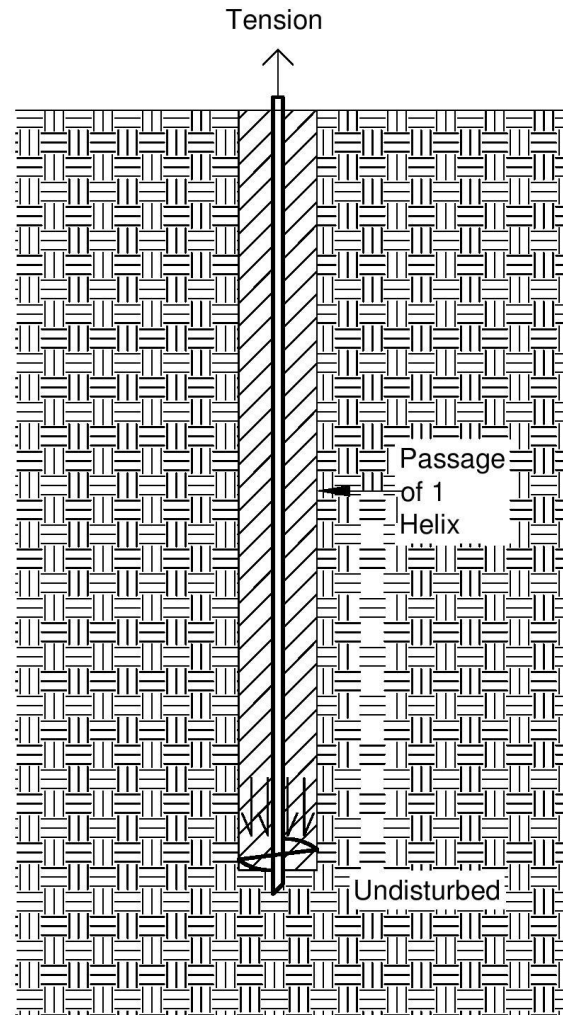
“Cemented” Soils

“Sensitive” Soils

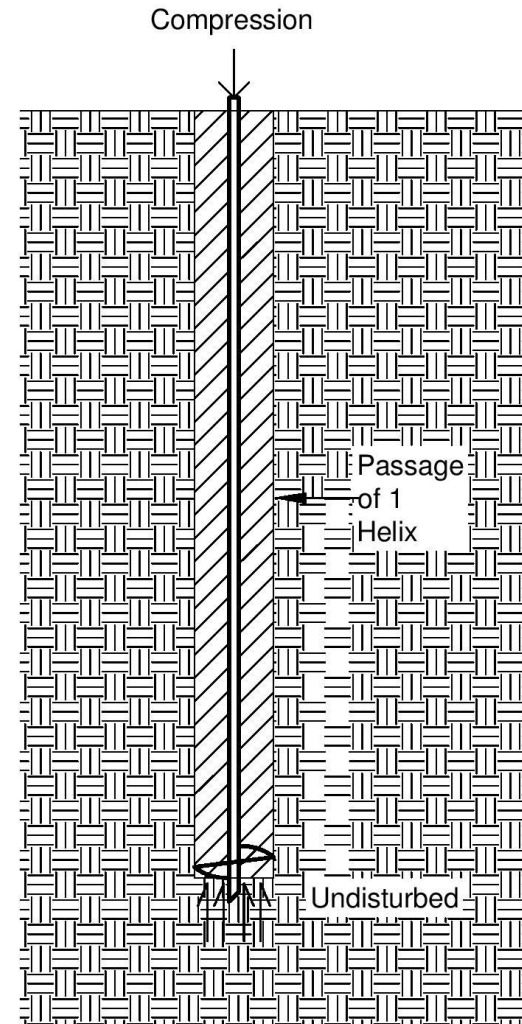
Dense Sands

All Soils?

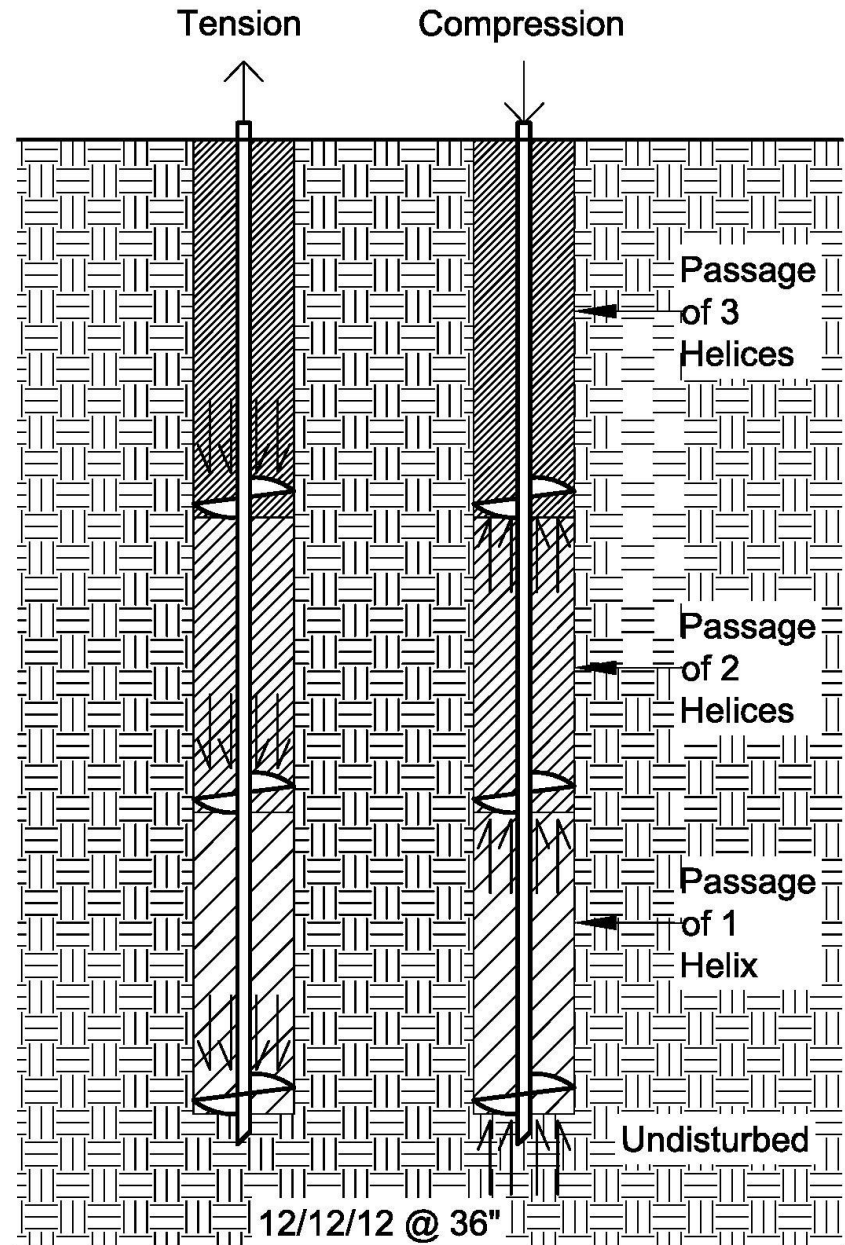
Tension Loading of Single-Helix in Clay



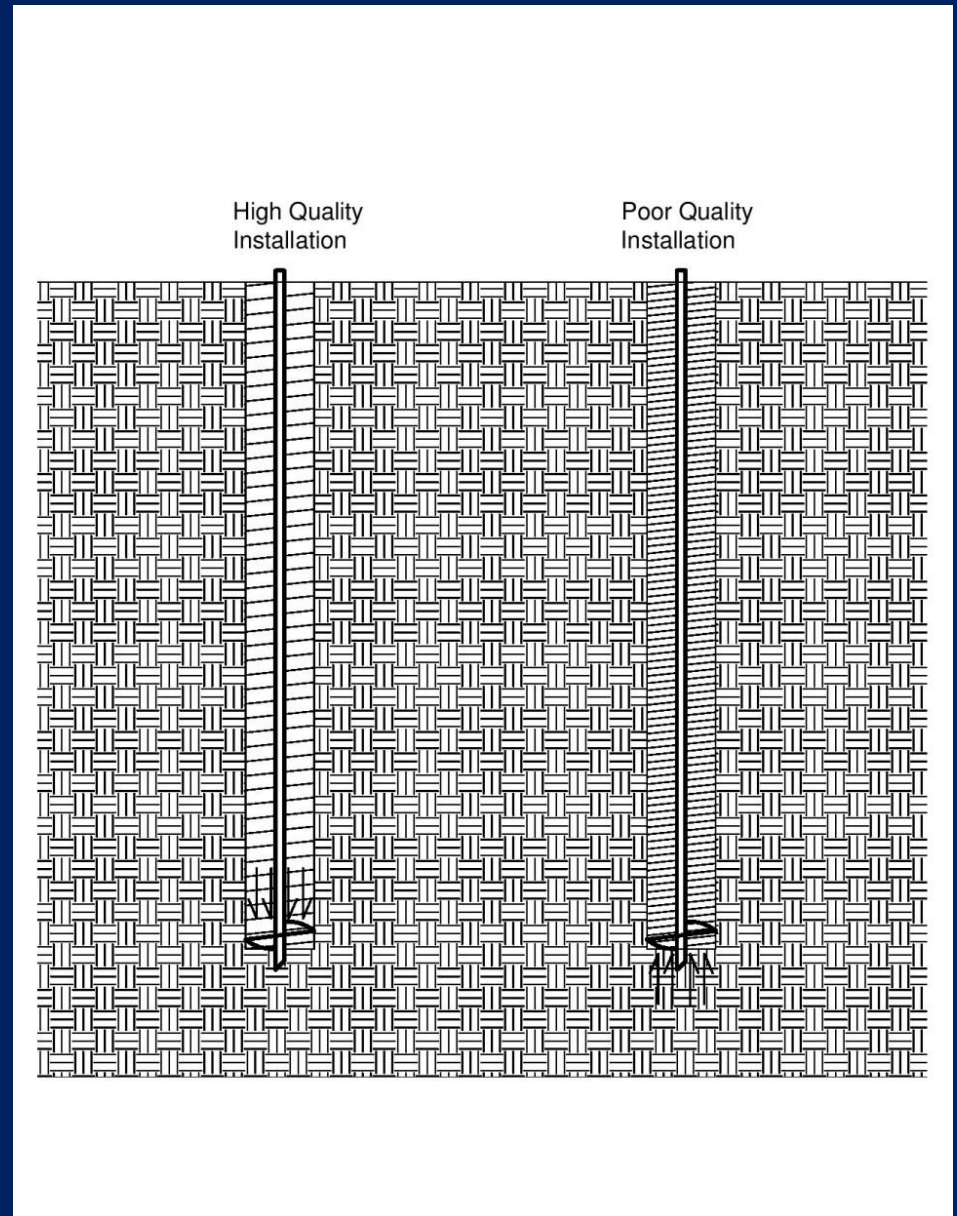
Compression Loading of Single-Helix in Clay



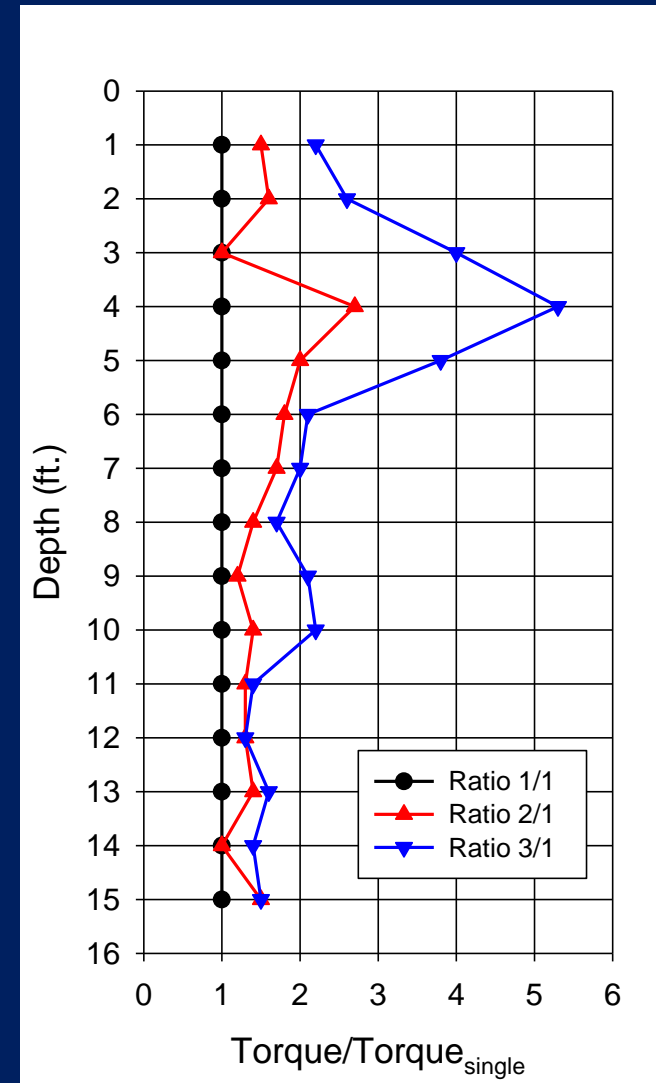
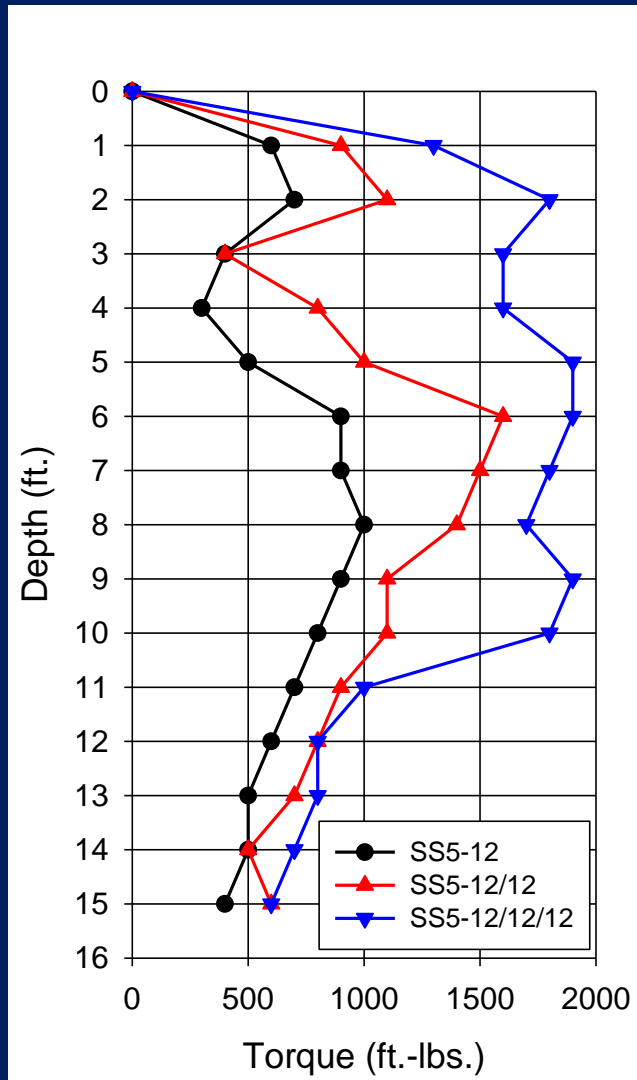
Tension and Compression Loading of Multi-Helix in Clay



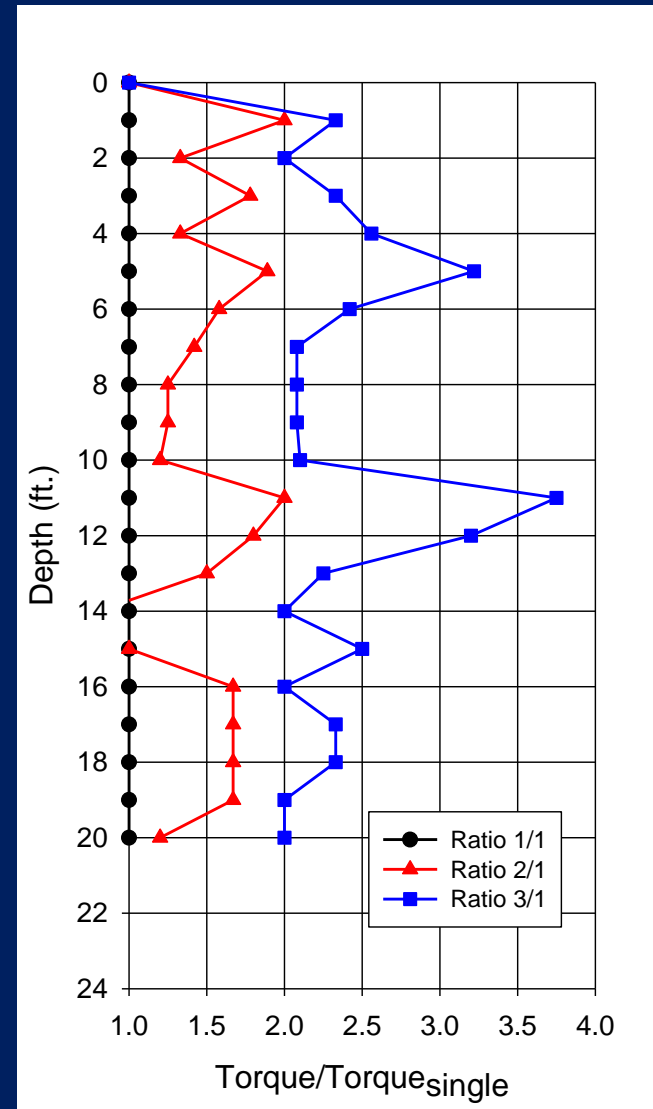
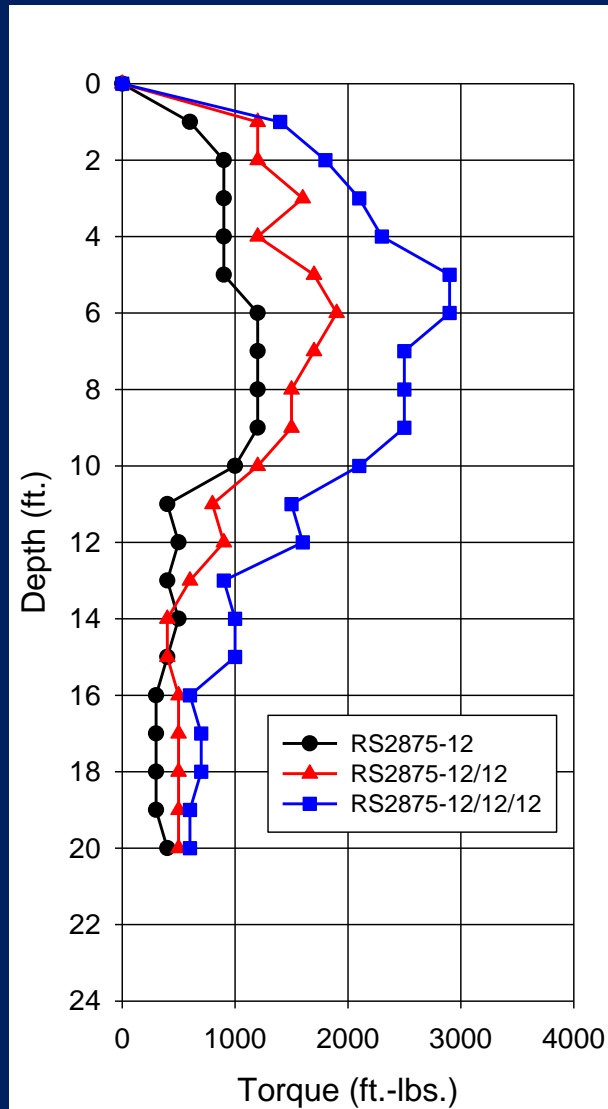
High Quality vs. Poor Quality Installation in Clay



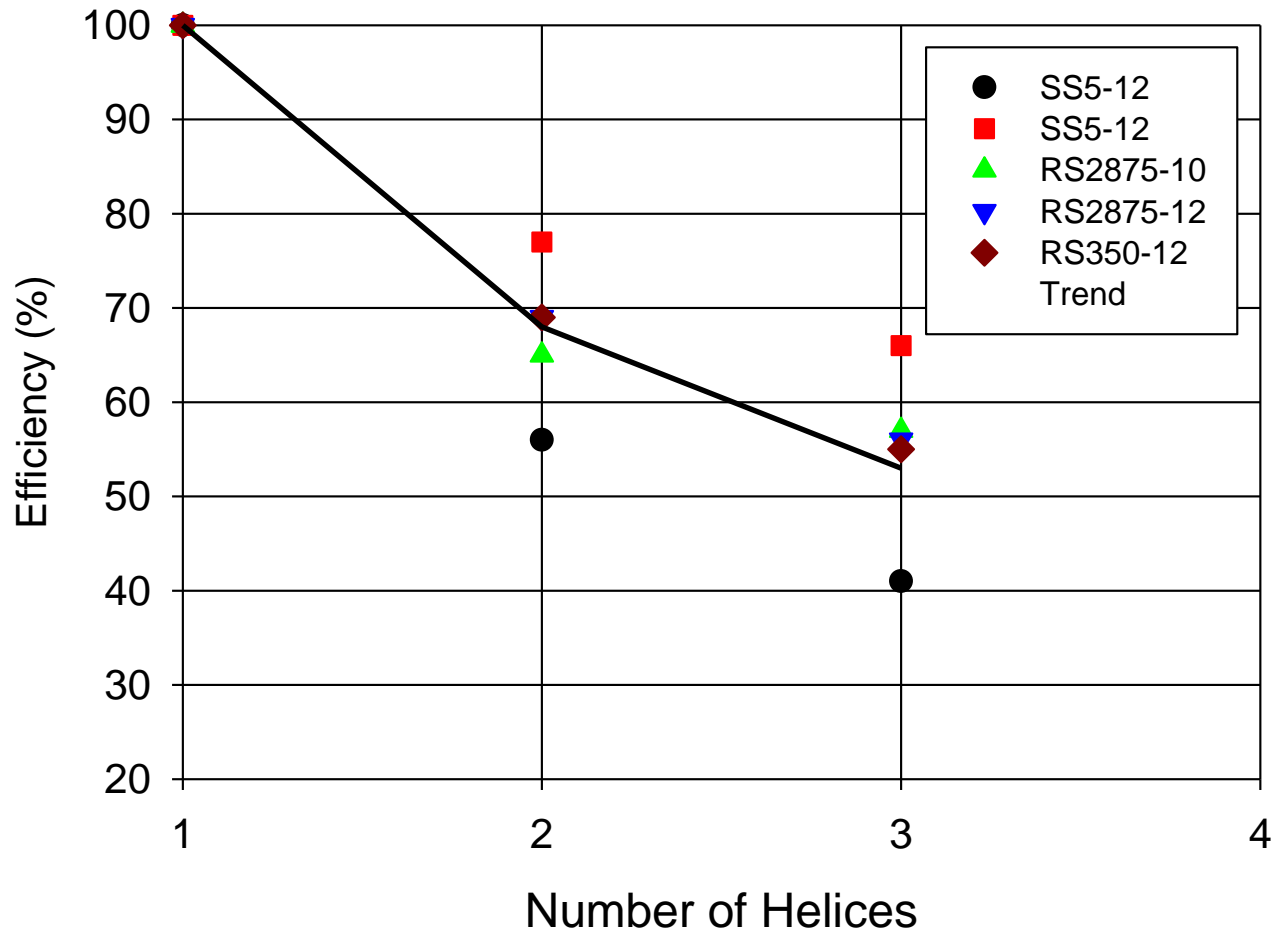
Square-Shaft Single- & Multi-Helix - Clay



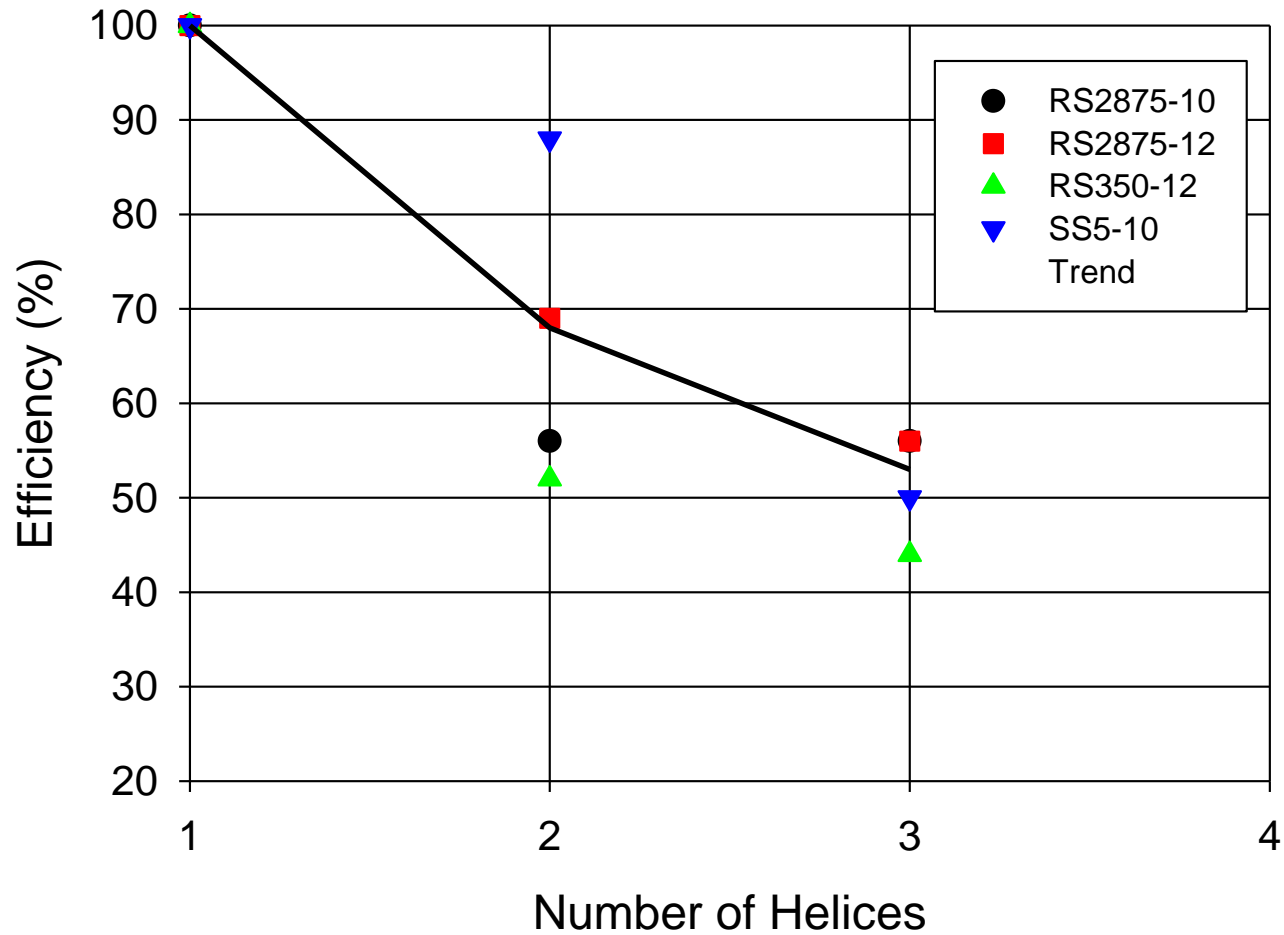
Round-Shaft Single- & Multi-Helix - Clay



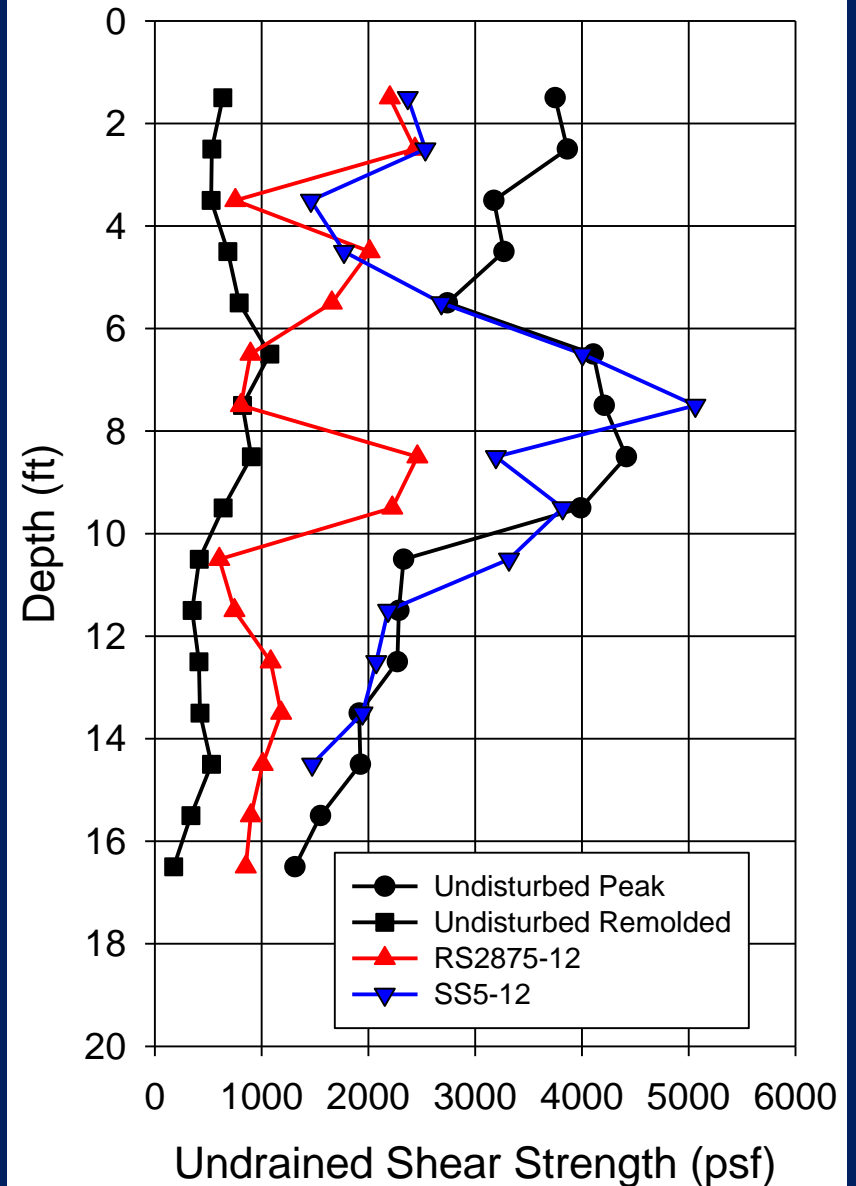
Soft Clay



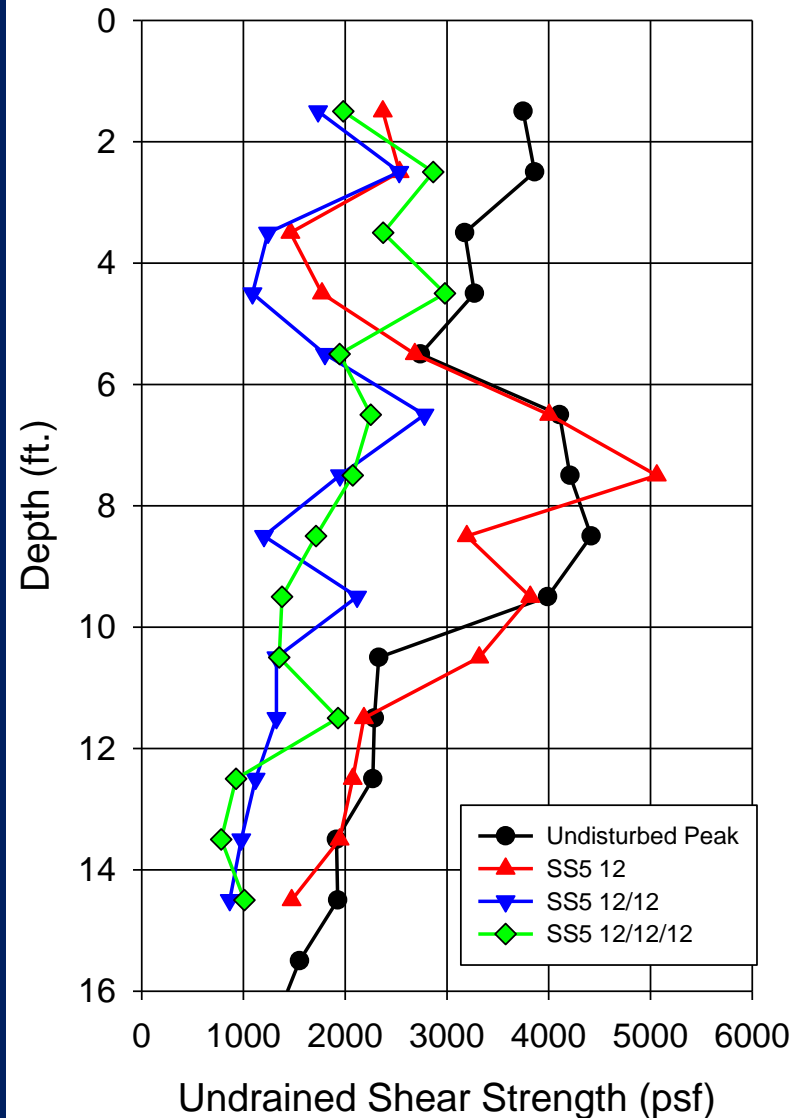
Stiff Clay



Vane Shear Tests Over Round-Shaft and Square-Shaft Single-Helix Anchors in Clay



Vane Shear Tests Over Square-Shaft Single- Double- and Triple-Helix Anchors in Clay



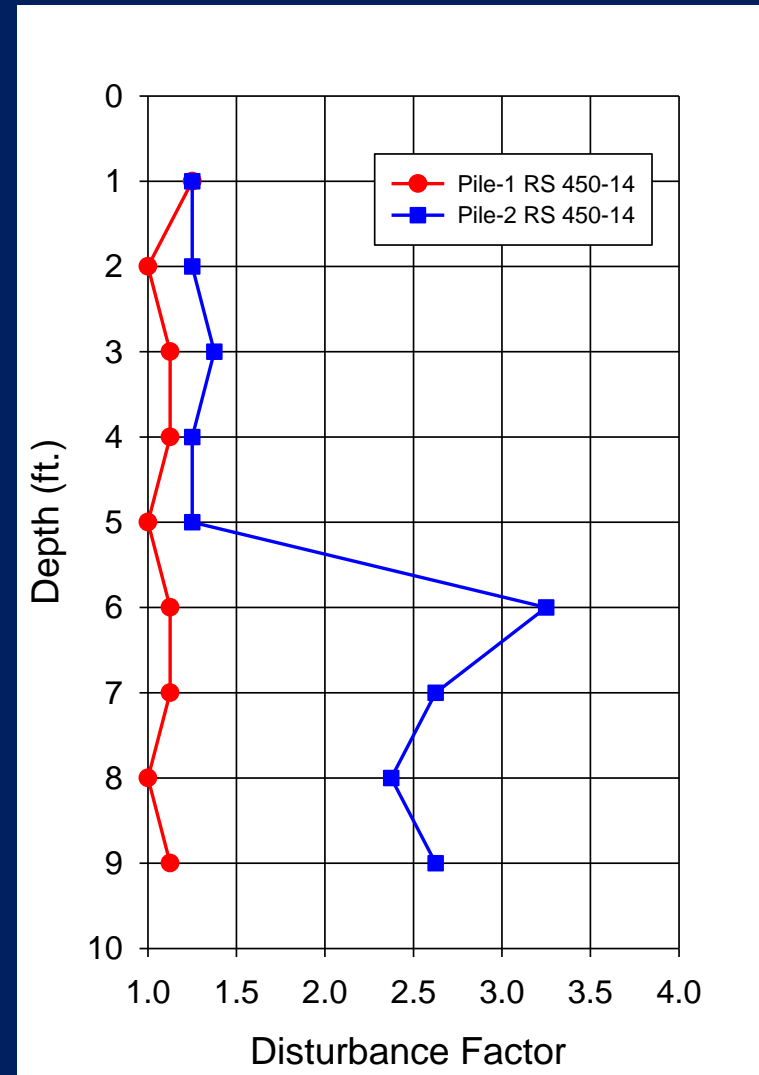
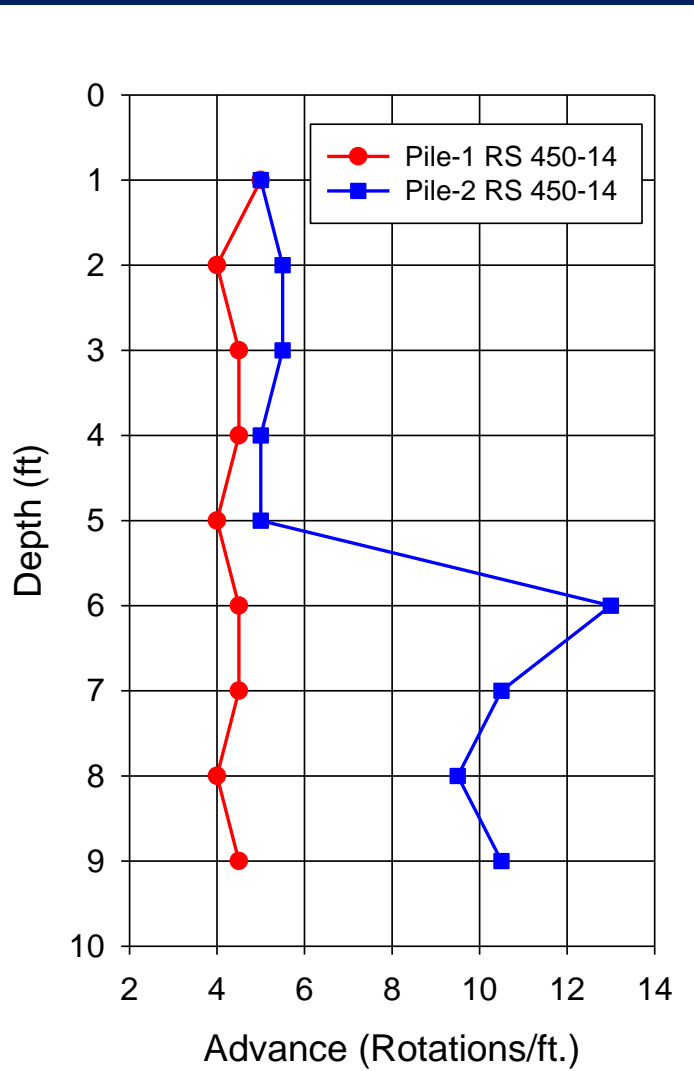
“Installation Disturbance Factor”

$$\text{IDF} = (\text{Rotations per Advance}) / (\text{Ideal Advance/Pitch})$$

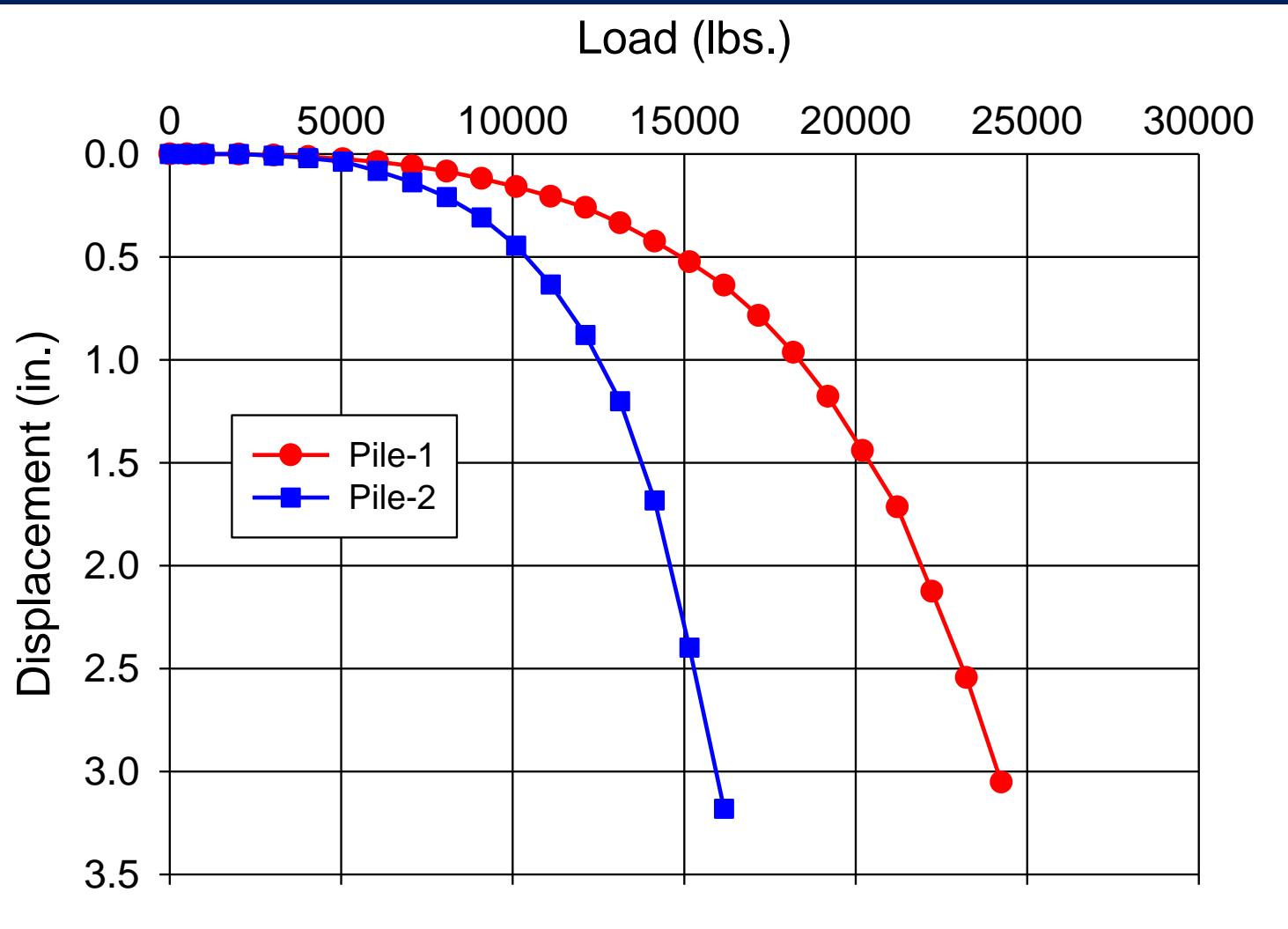
For Ideal or “Perfect” Installation of
Screws with a 3 in. Pitch

$$\text{IDF} = 4/4 = 1$$

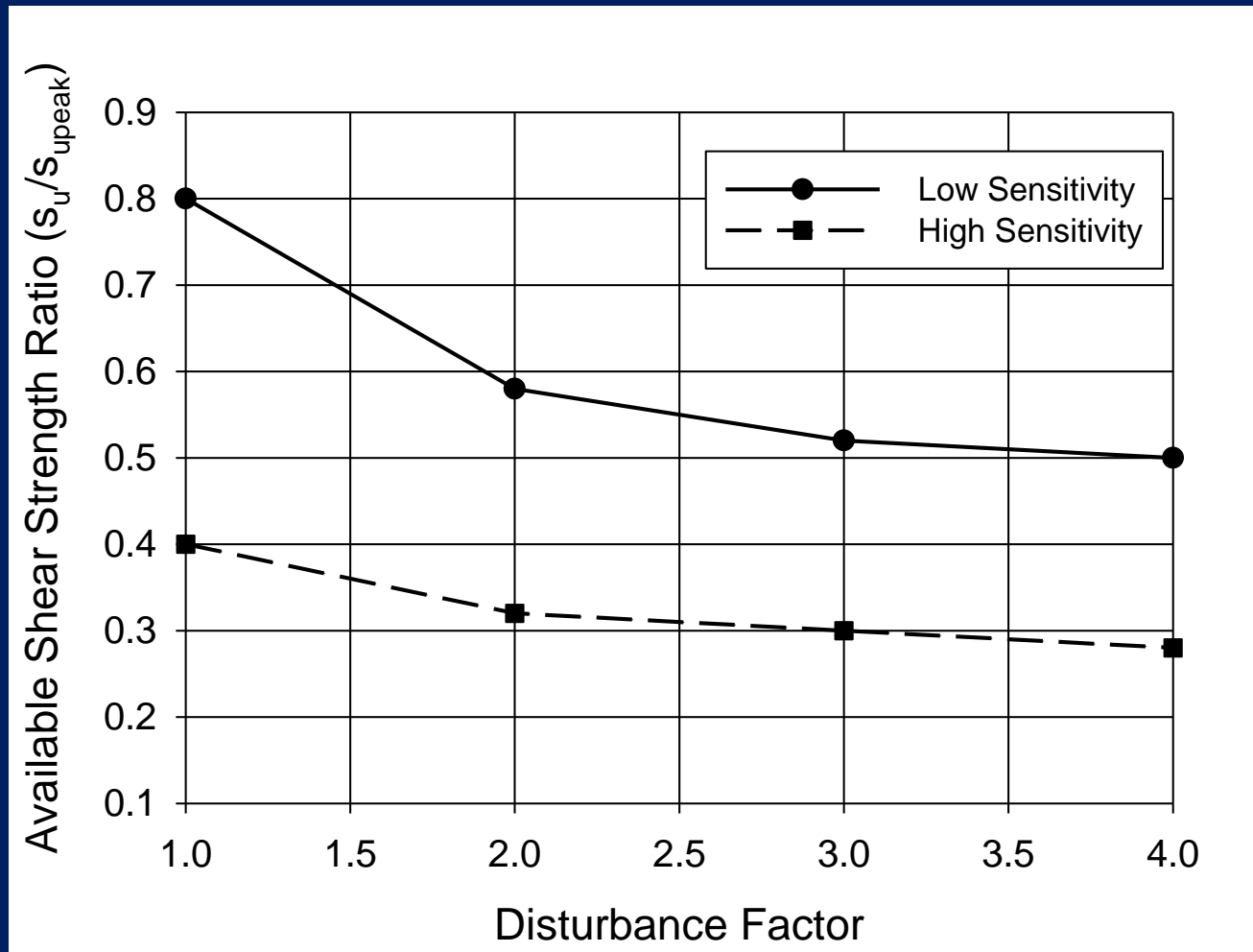
Measured Disturbance Factor - Clay



Influence on Load Test Results



For Clays We Might Want to Relate Available Strength to IDF



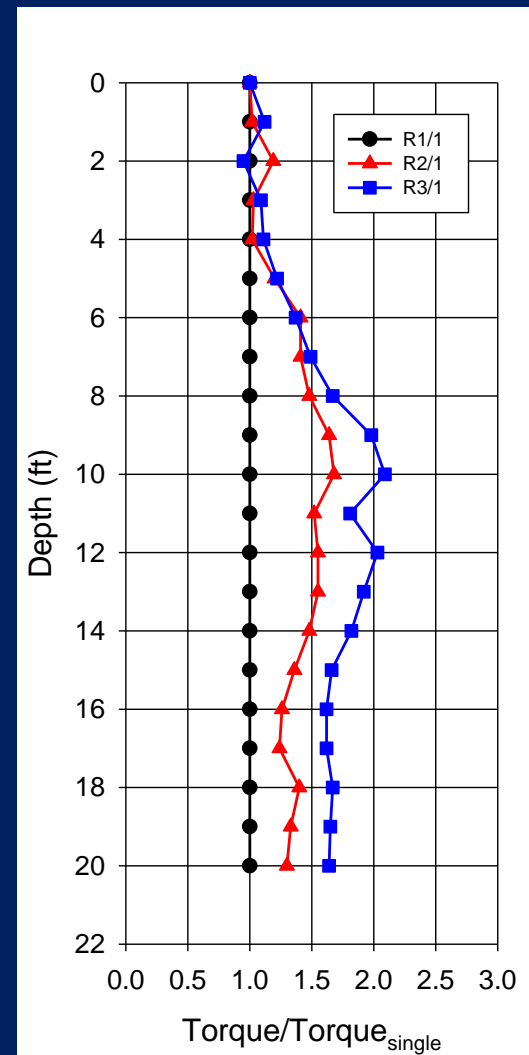
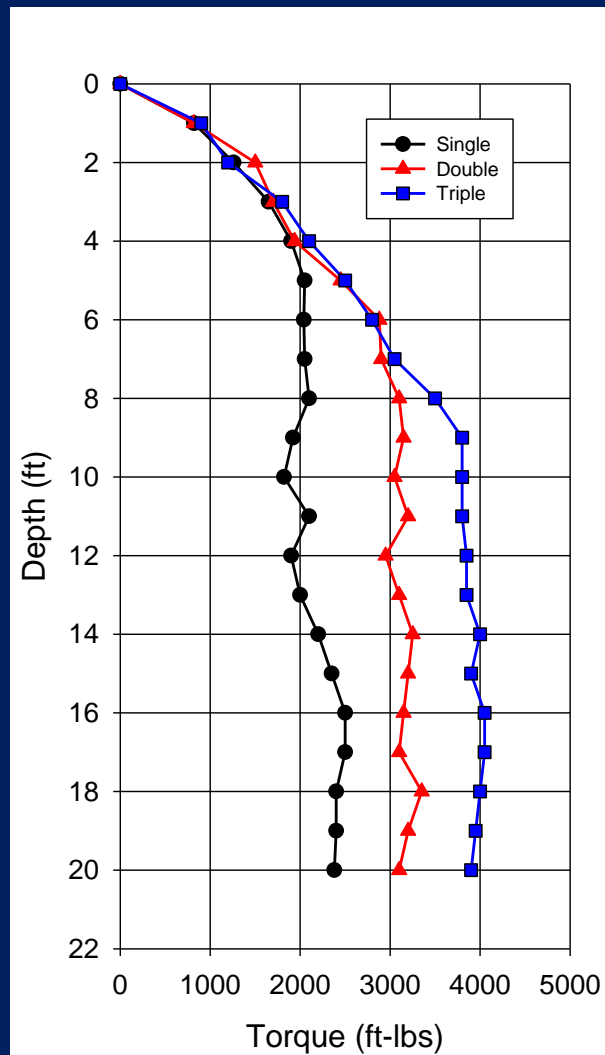
Skempton (1950)

Referring to triple-helix screw-piles in compression;

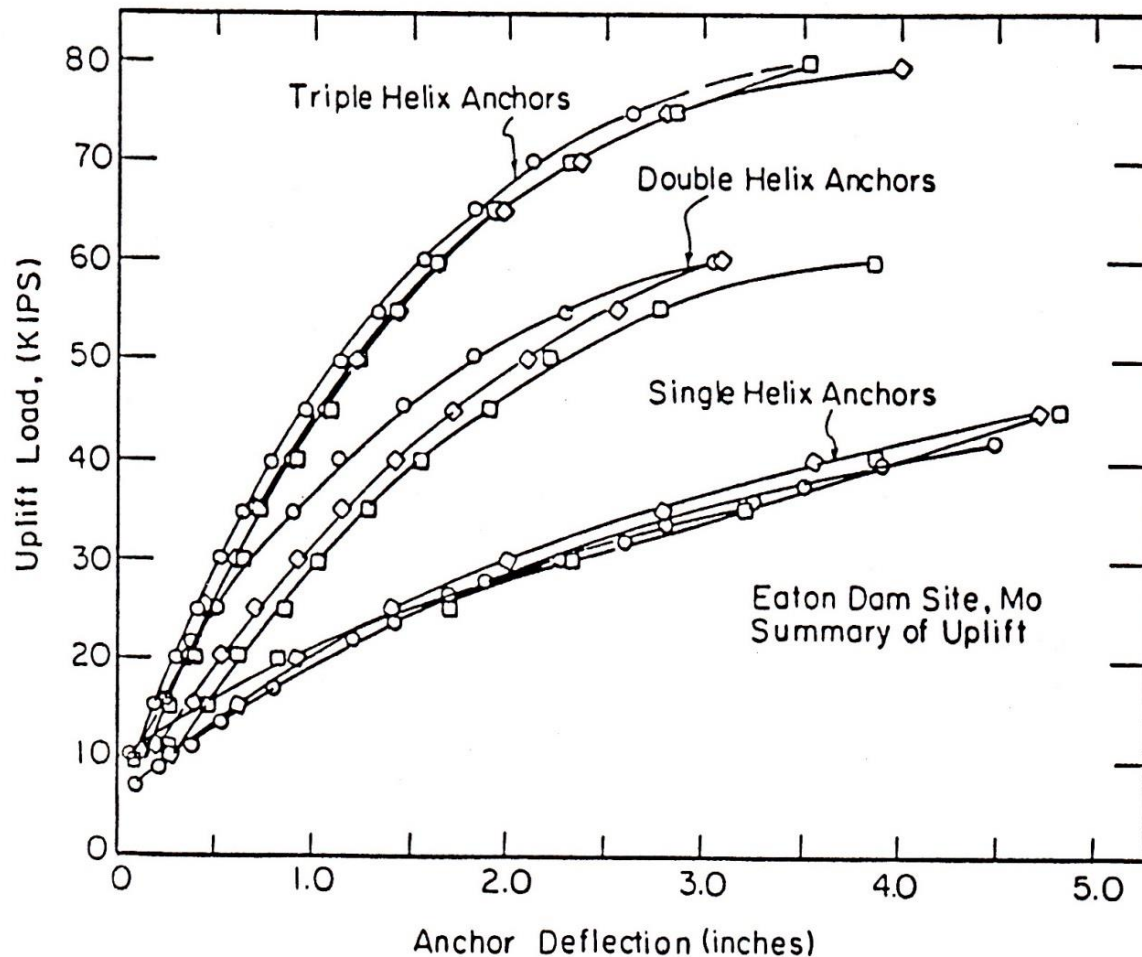
“...For Mr. Morgan’s double and triple screw-cylinders, it was necessary to recognize that the clay beneath the upper screws had been remoulded by the passage of the first screw. However, the whole of the volume of the clay contributing to the bearing capacity of the upper screws would not be fully remoulded and, as a rough approximation, it could be assumed that the average shear strength of the volume of clay was equal to:

$$c_{p2} = c - \frac{1}{2}(c - c_r)$$

Torque Profiles in Sand (Clemence et al. 1994)



Single, Double and Triple Helix Anchors in Sand (Clemence et al. 1994)



Installation of Screw-Piles and Helical Anchors Causes Disturbance to the Soil

The Degree of Disturbance will Depend on a Number
of Factors, Including: Soil Initial State, Sensitivity &
Installation Quality

Using IDF Requires Monitoring Installation

Challenge 3. Understanding Role of Shaft for Large Round Shaft Screw-Piles and Helical Anchors

Somewhat Unique to Screw-Piles and Helical
Anchors but Important for Many Deep
Foundations

We Need to Evaluate How Design Load is
Carried

What is the Role of the Shaft?

Transfer Load To Helix?

Provide a Component of Load
Capacity?

Load Distribution in Deep Foundations (% End vs. % Side)

Depends on:

Pile Type & Use

Installation Method

Geometry (L/D)

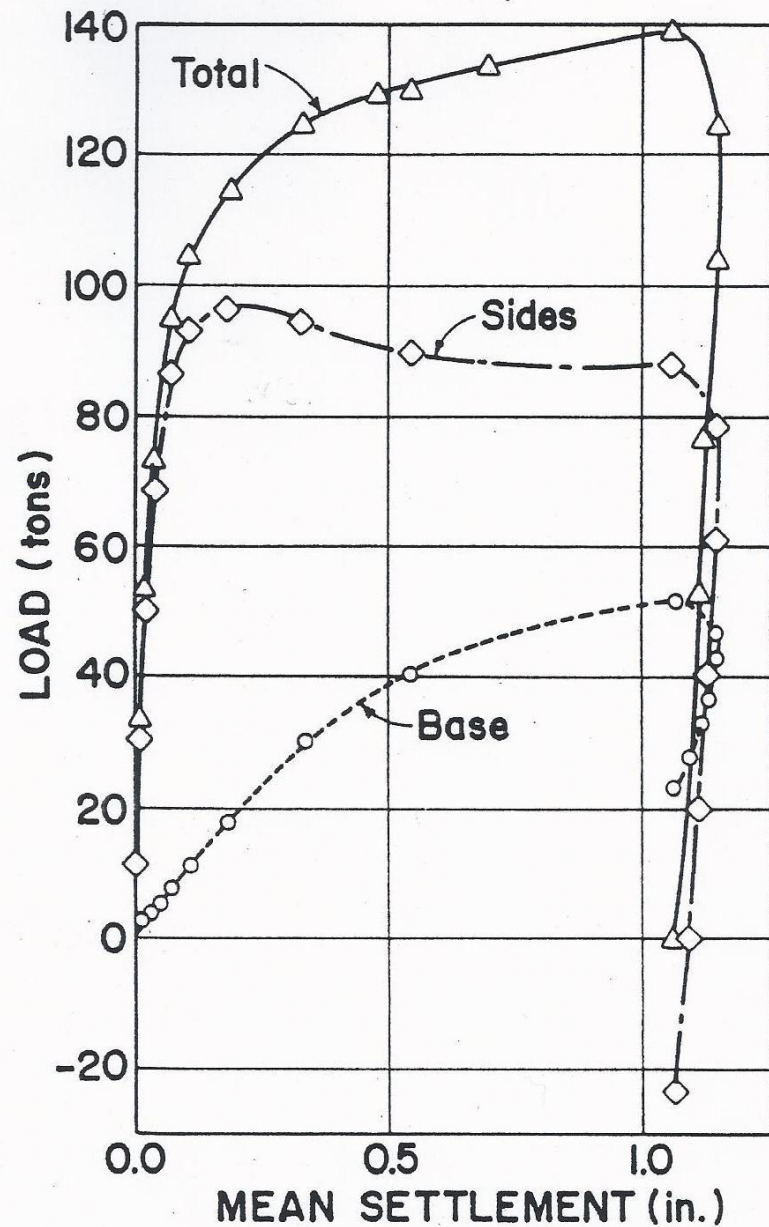
Soil Type

Stratigraphy

Load Level (Relative to Ultimate)

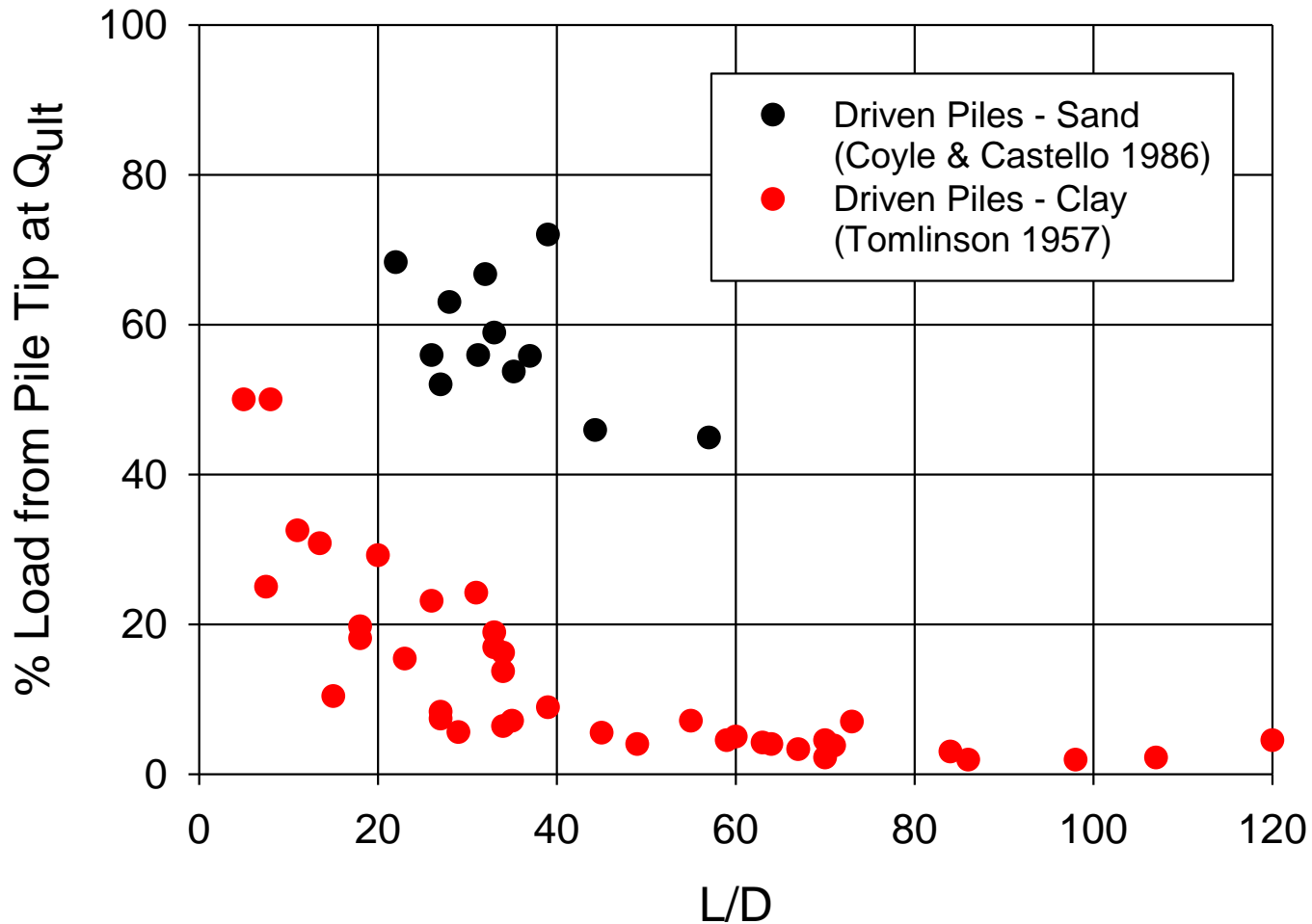
End and Side Don't Develop Capacity at the
Same Rate

Reese et al. 1976



At Q_{ult}
36.8% End Bearing;
63.2% Side
Resistance
At $Q_{ult}/2$
5.7% End Bearing;
94.3% Side
Resistance

Observed Distribution @ Q_{ult}



Parametric Analysis of Contribution of Shaft in Clays – Round Shaft Single Helix in Tension

$$Q_T = Q_H + Q_S$$

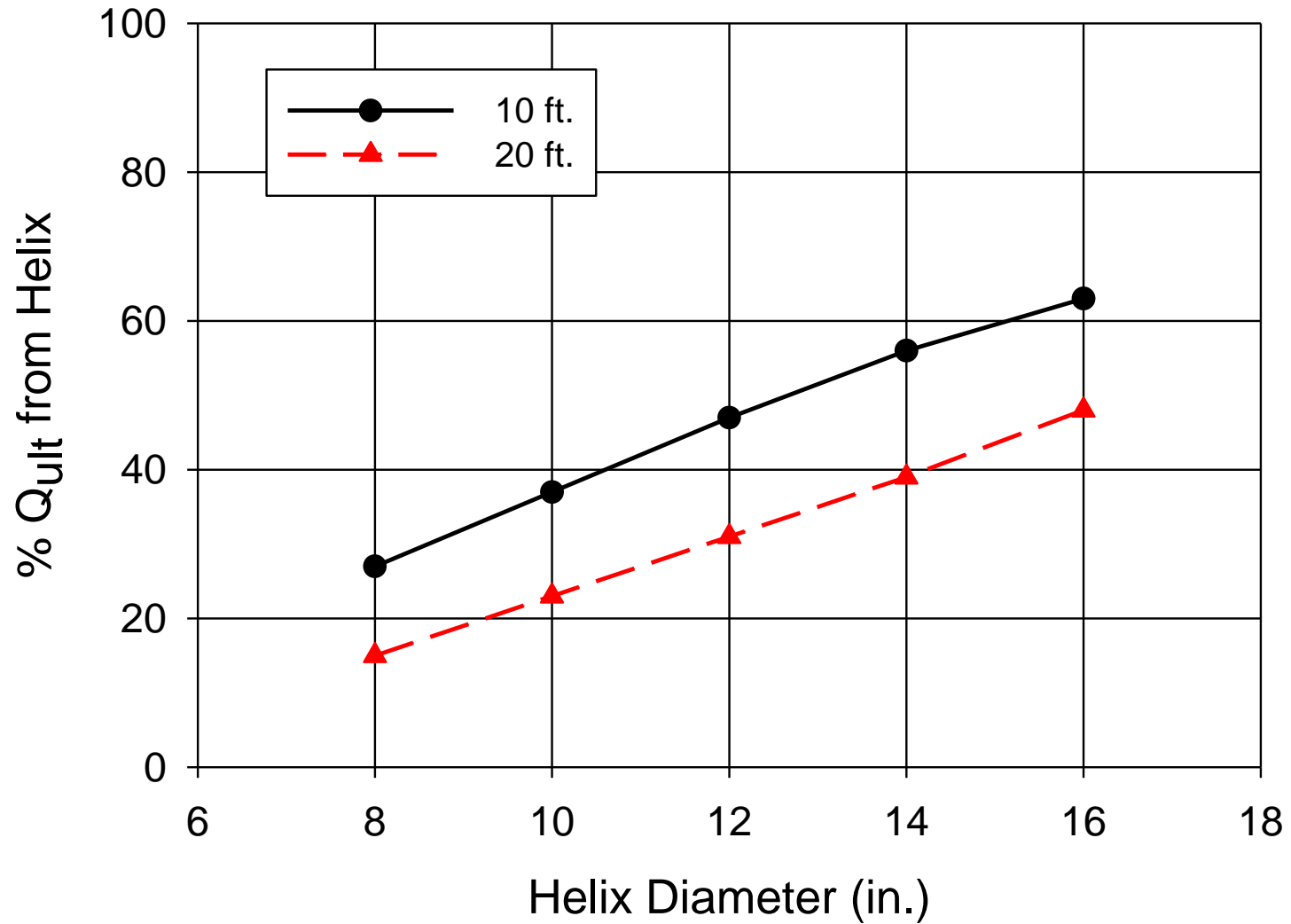
$$Q_H = s_u 9 A_H \quad Q_S = f_s A_S$$

$$f_s = s_u \alpha$$

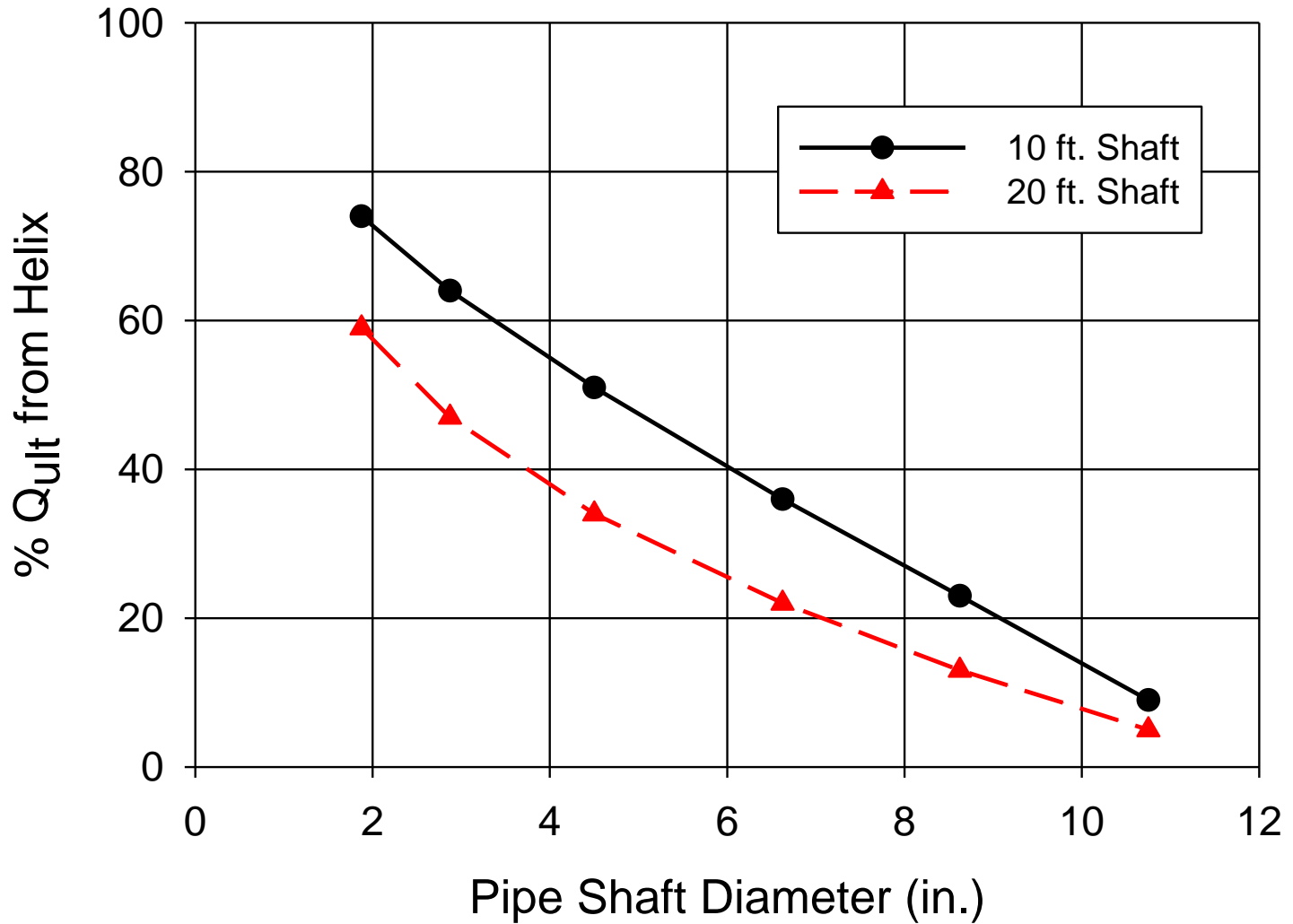
“soft” clay $s_u = 500$ psf $\alpha = 1$ $S_t = 2$

“stiff” clay $s_u = 2000$ psf $\alpha = 0.5$

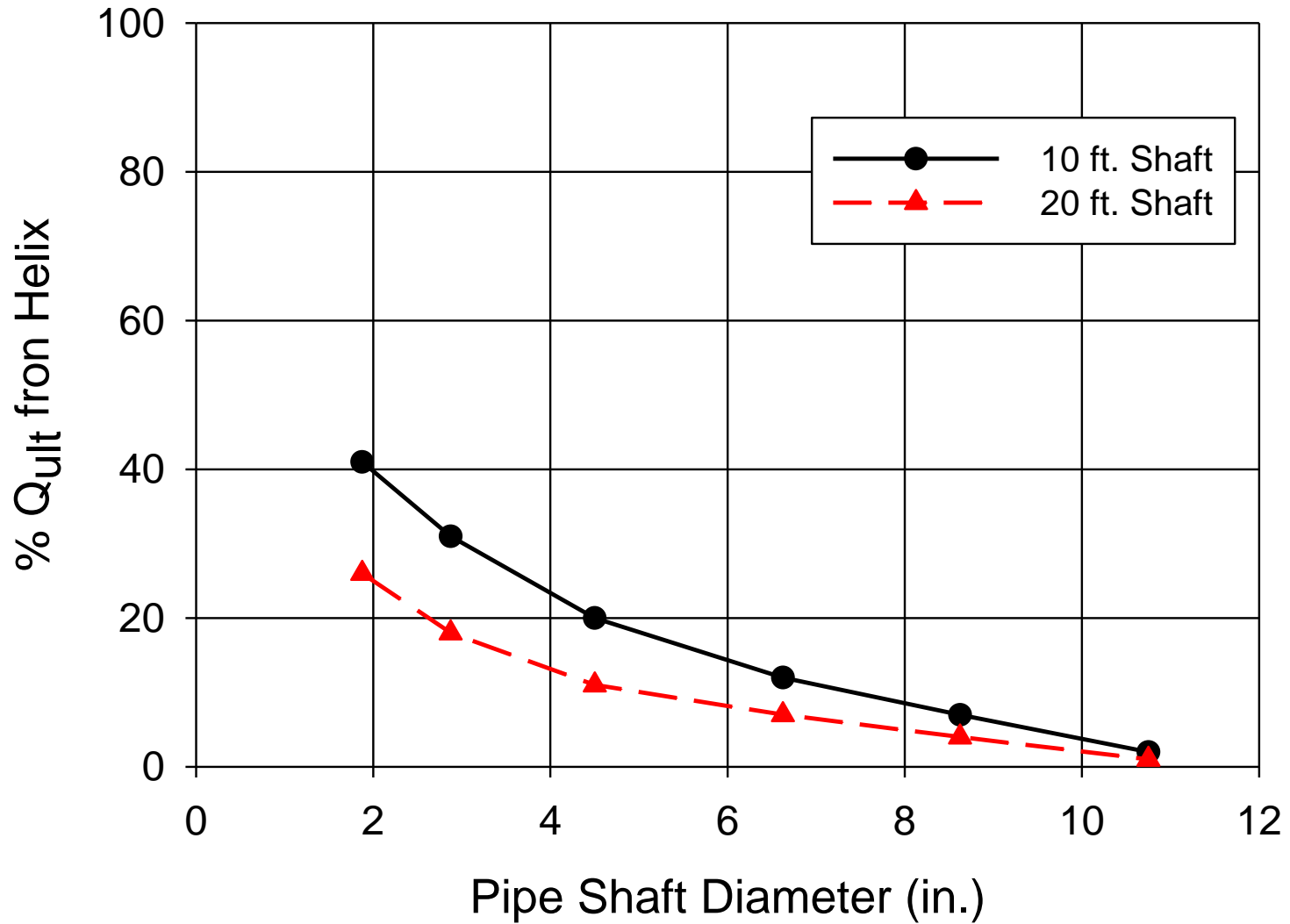
Soft Clay - 2.875 in. Diameter Shaft



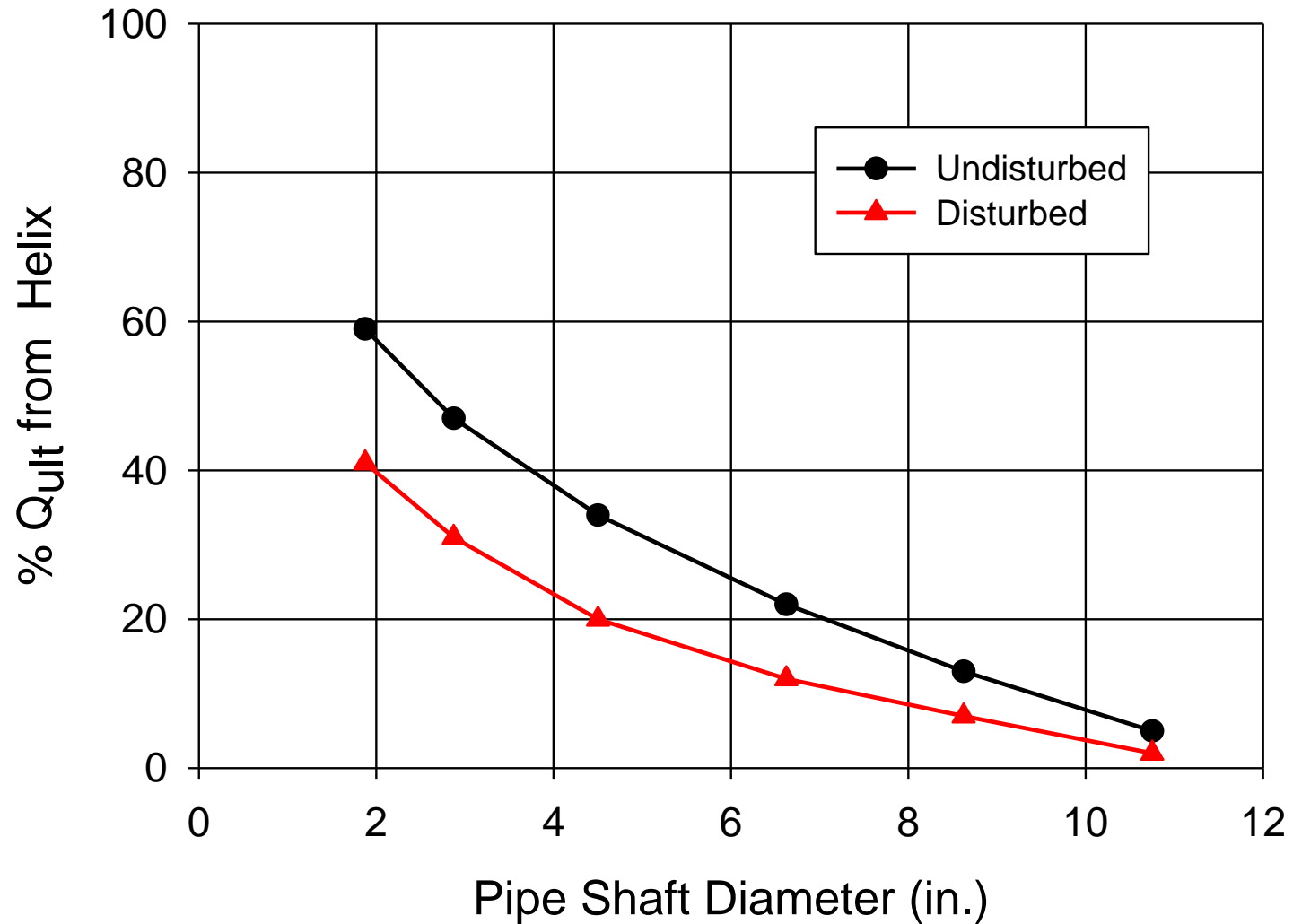
Stiff Clay - 12 in. Dia. helix



Soft Clay - 12 in. Diameter Helix Disturbed



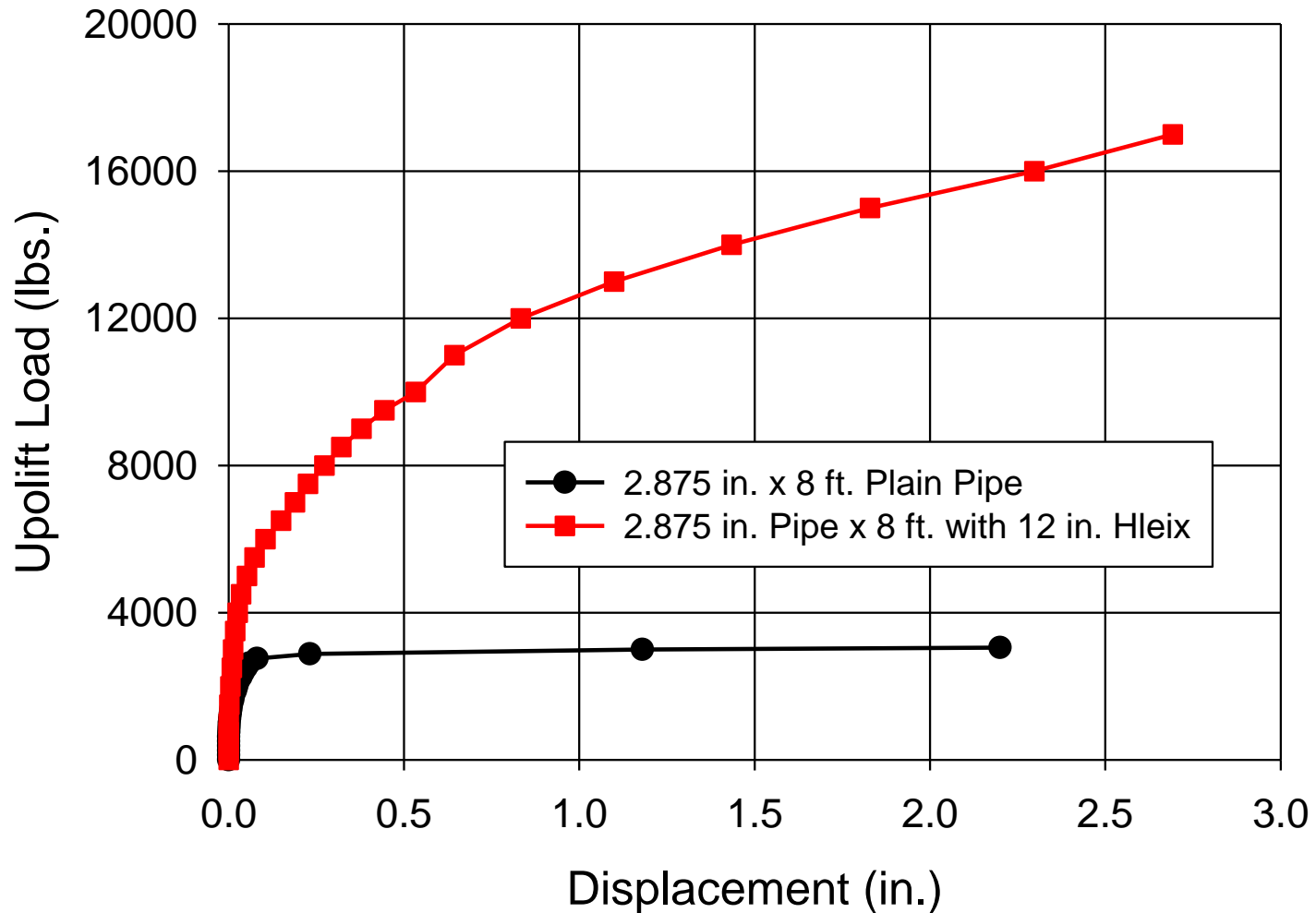
Soft Clay - 12 in. Diameter Helix 10 ft. Shaft

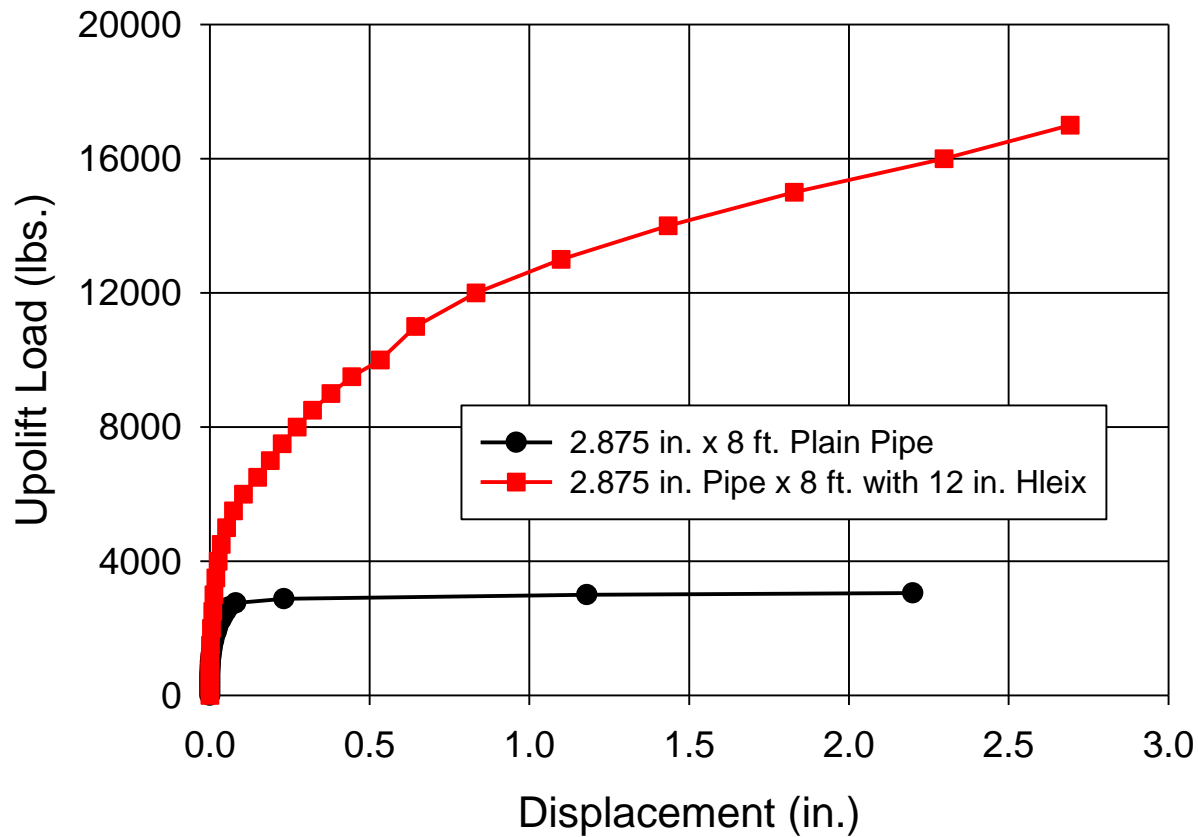


Single-Helix Pipe Piles in Uplift

Load Tests to Failure on Helical Pile and
Adjacent Plain Driven Pipe Pile

Stiff Clay - 2.875 in. Pipe



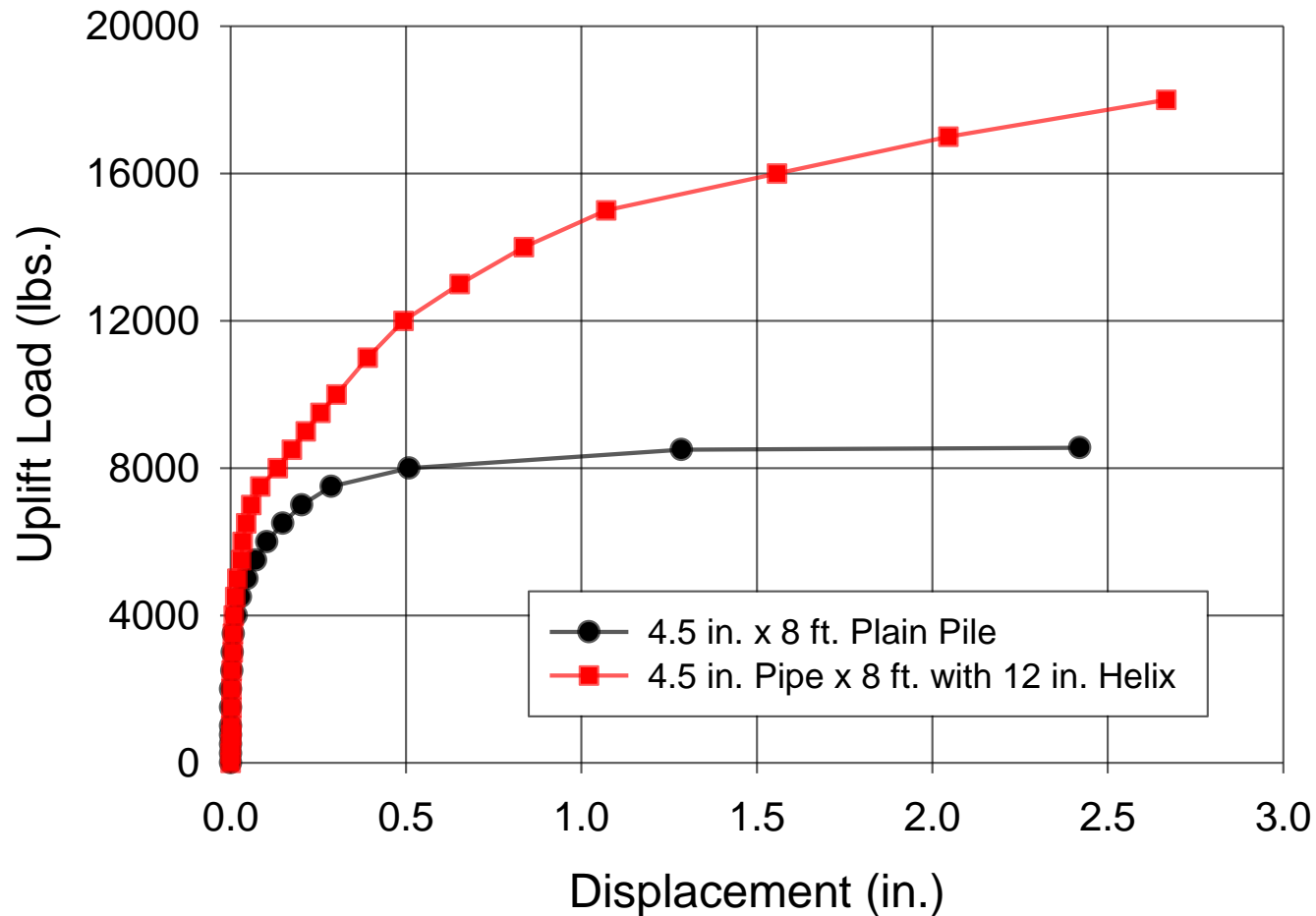


$$Q_{20} = 16,400 \text{ lbs.}; \quad Q_{10} = 13,200 \text{ lbs.}$$

$$Q_{10}/Q_{20} = 0.80 \quad \Delta @ Q_{10}/2 = 0.18 \text{ in.}$$

$$@ Q_{10} \quad Q_{\text{shaft}} = 2600 \text{ lbs.}; \quad Q_{\text{helix}} = 10,600 \text{ lbs.}$$

Stiff Clay – 4.5 in. Pipe



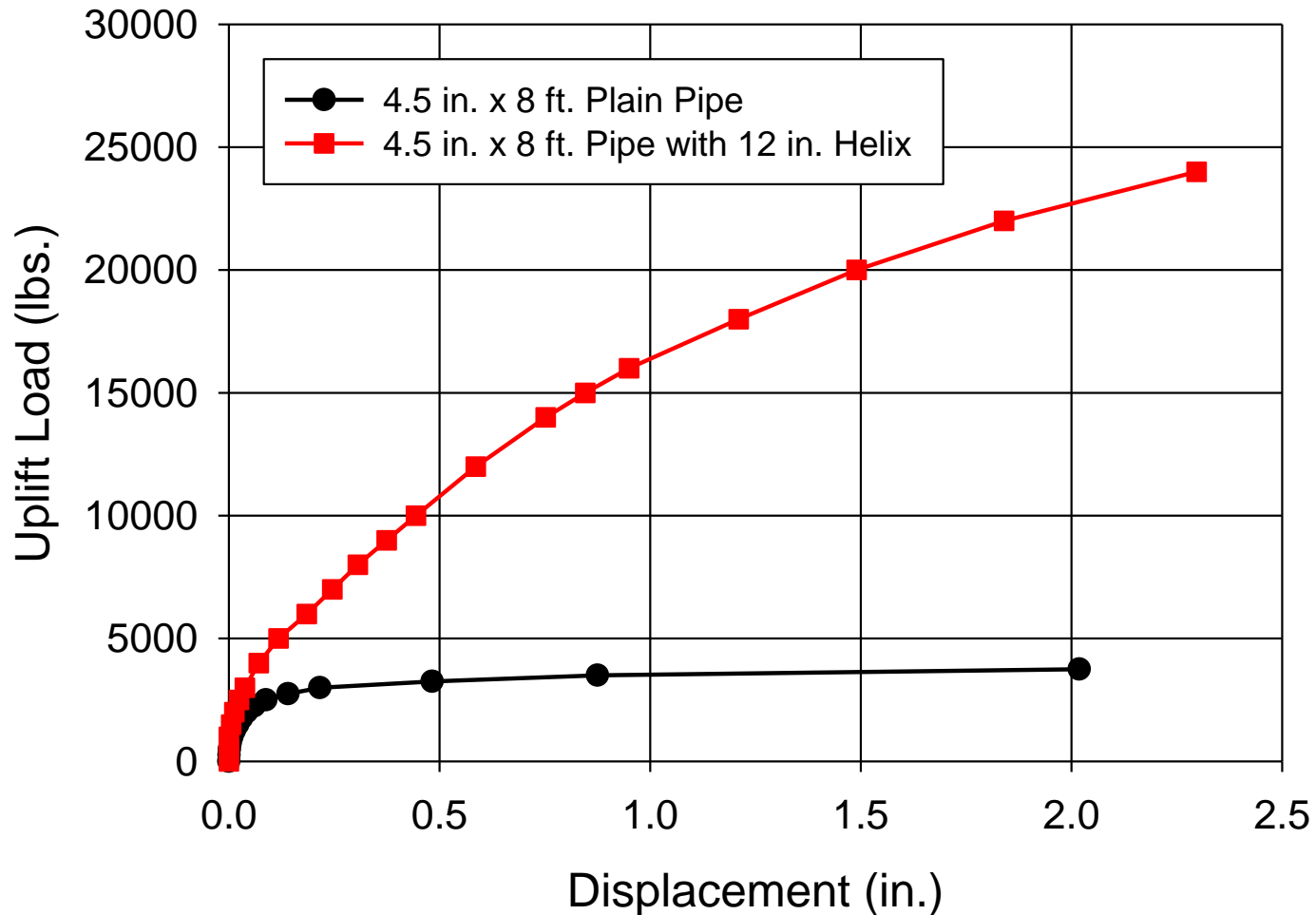
Distribution of Q_{shaft} & Q_{helix} at Q_{10} (Q in lbs.)

Pipe Dia.	Q_T	Q_S	Q_H
2.875	13,200	2600 (20%)	10,600 (80%)
4.5	15,250	8450 (55%)	6800 (45%)
6.625	20,000	10,600 (53%)	9400 (47%)

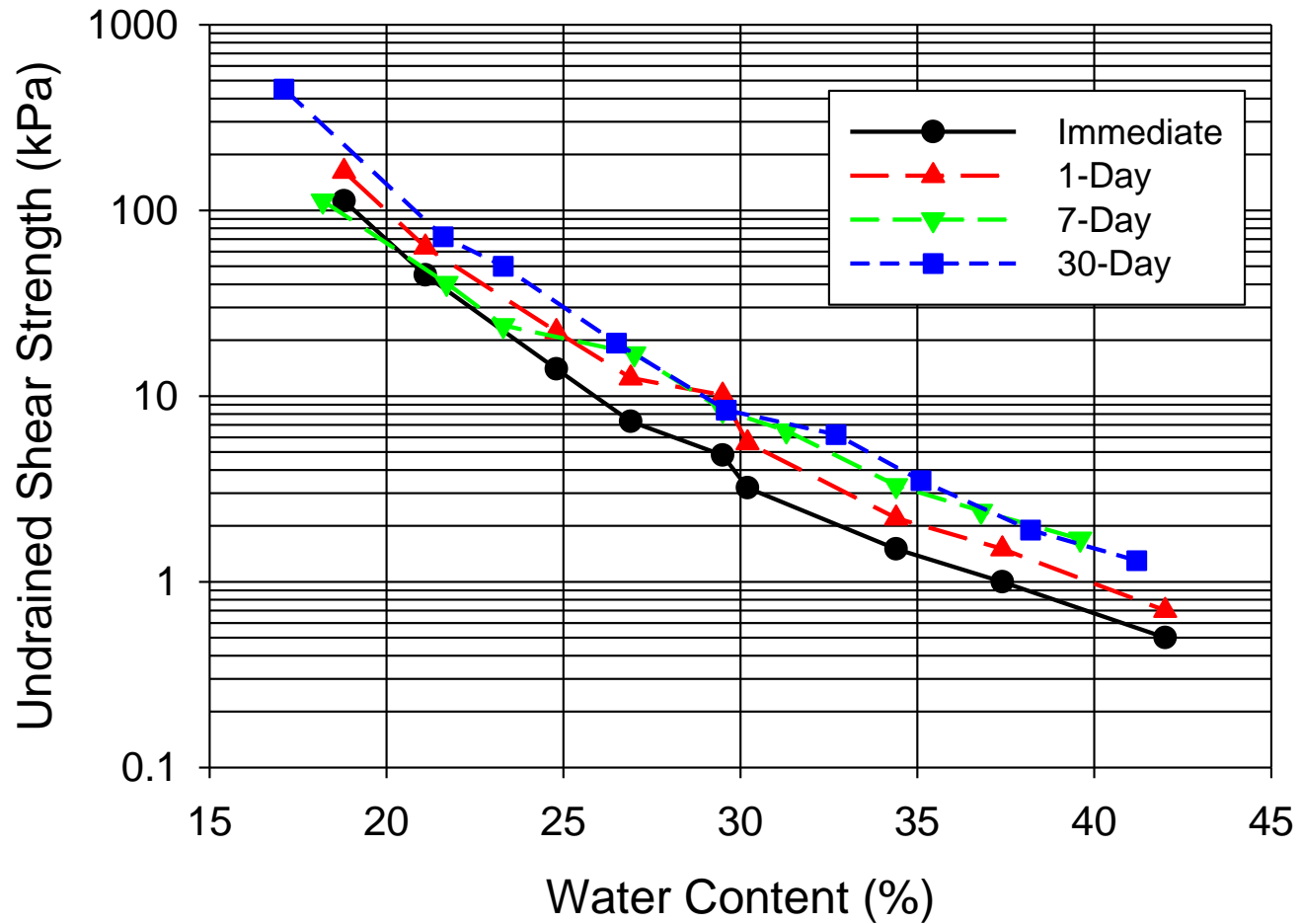
Distribution of Q_{shaft} & Q_{helix} at $Q_{10}/2$ (Q in lbs.)

Pipe Dia.	Q_T	Q_S	Q_H
2.875	6600	3000 (45%)	3600 (55%)
4.5	7625	6100 (80%)	1525 (20%)
6.625	10,000	6500 (65%)	3500 (35%)

Silty Sand



Aging ?



Summary

1. The Behavior of Screw-Piles and Helical Anchors is More Complex than has Previously Been Considered
2. Evaluation of Soil Parameters for Design Must Consider Installation Disturbance
3. Design Methodologies will Need to Change to Reflect These Considerations
4. Installation Monitoring of both Torque and Advance is Essential
5. As Industry moves to Large Diameter Pipe Shafts, the Role of the Helix Changes

Torque-to-Capacity Correlations?

The Logic

$$Q_{\text{ult}} = f(\text{Soil Properties \& Pile/Anchor Geometry})$$

$$T = f(\text{Soil Properties \& Pile/Anchor Geometry})$$

$$Q_{\text{ult}} = TK_t$$

But... K_t Depends on a Number of Factors Because
Torque Depends on a Number of Factors

Pile/Anchor Factors

1. Helix Diameter
2. Number of Helices
3. Helix Pitch
4. Surface Roughness
5. Helix Thickness
6. Shaft Shape (S/R)
7. Connection Style

Soil Factors

8. Soil Type

9. Soil Strength

10. Soil Stiffness

11. Soil Sensitivity

12. Water Table (sat. vs. unsat.)

Contractor (Installation) Factors

13. Rotation Rate

14. Advance Rate

15. Down Force (Crowd)

16. Inclination

Measuring Torque - Direct Methods



Monitoring Installation is Critical to Performance

Installation Torque

Installation Advance (rev/ft.)

International Society for Helical Foundations (ISHF)

www.helicalfoundations.org

